

# **THERMO UTILITIES**

# **MS EXCEL ADD-INS**



**Version 3.5 for 32-bit Excel 97-2003, 2007, 2010 and higher**

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Release Date: June 24, 2013

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## Update and Upgrade History

### **Upgrade note for version 3.5, release date June 15, 2013**

- *Compatibility with latest release of Excel, Win 7 and Win 8*
- *Fluid Properties is now a freeware.*
- *The database interface of fluid properties are replaced with table look up.*

### **Upgrade note for version 3.0, release date Jan. 12, 2000**

- *Adding Lee-Kesler method to the package.*
- *Adding a database with properties of more than 450 chemicals*

### **Update note for version 2.05, release date Jan. 25, 1999**

*Optimizing stmxl.dll*

### **Update note for version 2.03, release date Dec. 30, 1998**

*Bug fixes in unit.xla*

### **Update note for version 2.02, release date Sept. 30, 1998**

*Bug fixes*

### **Release note for version 2.01, release date Sept. 14, 1998**

*Support for MS Excel 7, 97, Office 97 and higher (32-bit)*

### **Release note for version 2.0, release date Sept. 10, 1998**

*Thermo Utilities v2.0 is a software package developed for engineers and scientists, who wish to design, analyze or optimize power plants and air conditioning systems. It supports MS Excel 5.0 (16-bit) and it will run on PC platforms with operating systems, Win 3.1, Win 95, Win 98, Win NT 3.51 and higher.*

*It offers a large number of functions for calculating the properties of water, steam, air and flue gases. The functions used for steam and water properties are based on a set of equations accepted by the members of the Sixth International Conference on the Properties of Steam. The sets of equations are also known as "IFC Formulation for Industrial Use". Thermo Utilities calculates the properties of dry air, moist air, exhaust and flue gases by using equations accepted by ASHRAE and CIBSE (Chartered Institute of Building Services Engineers).*

*The package also offers a large number of inverse functions which are useful for applied thermodynamics calculations. For more details see the help file that comes with this package.*

*The earlier version of this package has been offered as a bonus to the registered users of:*

- Steam properties v1.2 and higher
- Air and exhaust gas properties v1.2

## **Brief Description and Downloading**

Thermo Utilities v3.5 is a software package developed for engineers and scientists, who wish to design, analyze or optimize power plants, air conditioning systems and other chemical processes. It supports 32-bit version of MS Excel i.e. Excel 97-2003, Excel 2007, Excel 2010 and higher and it will run on PC platforms with operating systems Win XP, Vista, Win 7 and Win 8 and higher. We have supported older Excel version since 1995. If you need this application to run on older versions of Windows OS and Excel, please contact us.

Thermo Utilities offers a large number of functions for calculating the properties of water, steam, air, flue gases and other fluids. The functions used for steam and water properties are based on a set of equations accepted by the members of the Sixth International Conference on the Properties of Steam. The sets of equations are also known as "**IFC Formulation for Industrial Use**". Thermo Utilities calculates the properties of dry air, moist air, exhaust and flue gases by using equations accepted by **ASHRAE** and **CIBSE** (Chartered Institute of Building Services Engineers). **Lee-Kesler method** used in this package can be applied to a large number of chemicals for estimating thermodynamic properties. The database accompanied with this package for use with Lee-Kesler method supports more than 450 chemicals. The package also offers a large number of inverse functions which are useful for applied thermodynamics calculations. The features are:

- Support for VBA (Visual Basic for Application)
- User selectable units for inputs/outputs
- Calculates enthalpy, entropy, specific volume, dryness fraction, specific heat capacity, thermal conductivity, and dynamic viscosity
- All inverse functions, needed in applied thermodynamics applications, are provided. More about this can be found in the help files.
- Chemical compound database for: normal freezing point, normal boiling point, critical pressure, critical temperature, critical specific volume, critical compressibility factor, Pitzer's acentric factor, dipole moment, standard enthalpy of formation and Gibb's energy of formation.

Link for downloading the latest version: <http://www.taftan.com/tuxl30.zip>

There are also a number of worksheets (<http://www.taftan.com/xl/index.htm>) available for registered users. These worksheets cover combustion of coal, biomass and fossil fuel, compressor, condenser design, cooling with dehumidification, closed-feed heaters, gas turbine, mixing of two air stream, regenerative steam cycle, sensible cooling/heating process, steam turbine and steam valve/throttling process.

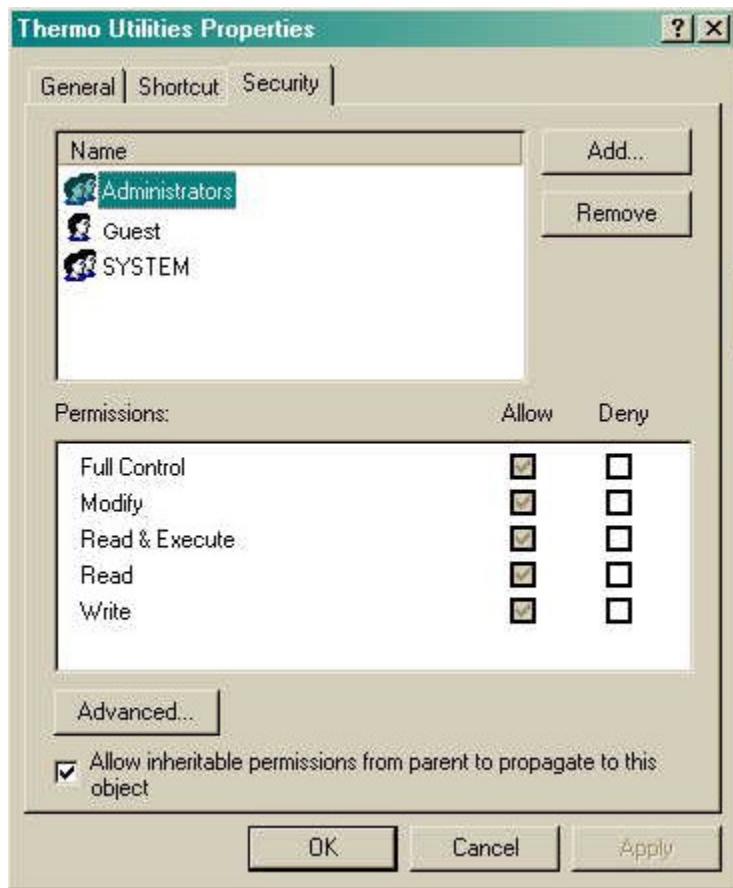
## **How to install Thermo Utilities**

You must have approximately 15.0 Mb of free disk space to install the program. Before you install "Thermo Utilities", please make sure that:

- You have installed the latest "Service Pack" for Windows operating system,
- You have installed the latest "Service Pack" for your "EXCEL" or "Office" software.

The installation procedure is as follows:

- In case, you need to login into your computer to use it, you should login as administrator to install the software.
- Copy "TUXL30.ZIP" to a suitable folder and unzip the file to folder "C:\THERMOXL"
- Attention: The software is made of many components. Each component search for other parts in the folder "C:\THERMOXL"
- Path to "Air and Flue Gas Properties" is: "C:\THERMOXL\AIRXL.XLA"
- Path to "Steam and Water Properties" is: "C:\THERMOXL\STMXL.XLA"
- Path to "Lee-Kesler method" is: "C:\THERMOXL\LKXL.XLA"
- Path to "Unit Conversion" is: "C:\THERMOXL\UNIT.XLA"
- Run "C:\THERMOXL\SetUnit.exe" and select the desired units.
- While you are logged in as administrator, you should give access to the software to all users that are allowed to use the software.



For doing this, click on Windows "start" button, select "Computer" then select "C:\THERMOXL" folder and then right click with mouse, select properties, select security, among the following options for the user (Full Control, Modify, Read & Execute, Read & Write) select "Full Control" and push "OK" button. The following instructions are Windows Vista only:

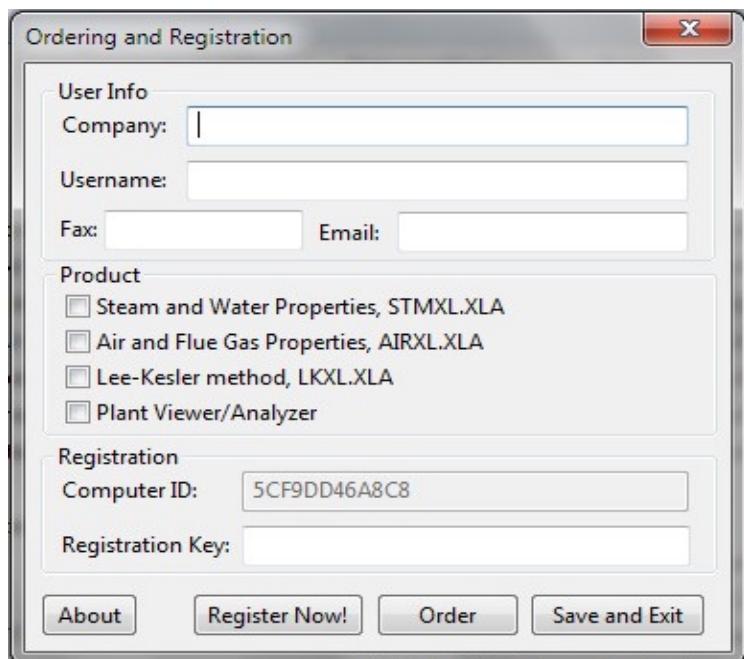
1. Click Start and Control Panel.
2. Switch to Classic View (if you haven't already) and click on the Administration Tools icon.
3. In the list that opens click on Local Security Policy, and in the next window, Local Policies (a tiny bit redundant, but all UIs can't be perfect -- If UAC is running you'll get a UAC pop-up somewhere in here).
4. In the Local Policies list click Security Options, and scroll down to "User Account Control: Behavior" (the full title of the policy is "User Account Control: Behavior of the elevation prompt for administrators in Admin Approval Mode" but the window barely opens that far).
5. Double-click the title and in the dialog box change its setting from "Prompt for Consent" to "Elevate without prompting."

## **How to Order Your Registration Key**

Before ordering your registration key, please check that everything works on your computer. Many functions of Thermo Utilities v3.5 should work even if you do not have a registration key. If there is any problem, do not hesitate to contact us. We solve all the problems, before you order our product. When you order you will receive your registration key that enables all the functions. It is not possible to transfer the registration key from one computer to other. If you wish to order your registration key, please run the program C:\THERMOXL\register.exe and:

1. Type your name, company name, fax number and your email address (blank if not applicable)
2. Select the Add-ins you wish to order
3. Press the Order button
4. Email us the software generated "order.txt". The file location is:  
"C\THERMOXL\order.txt"
5. Pay the registration fee

Here is a screenshot of ordering and registration utility:



## **How to Pay the Registration Fee**

The prices of the registration keys are:

- Air and Flue Gas Properties, MS Excel Add-ins 139 USD
- Steam and Water Properties, MS Excel Add-ins 149 USD
- Lee-Kesler method, MS Excel Add-ins 159 USD

In order to place your order, you need to visit our website at:

<http://www.taftan.com/thermoxl.shtml>

Once you click on the link for ordering, you will be connected to our order taking company SWREG. SWREG is a global cloud commerce solution. They offer numerous payment options and currencies, including phone and fax order support in many countries.

## **Finalizing the Registration**

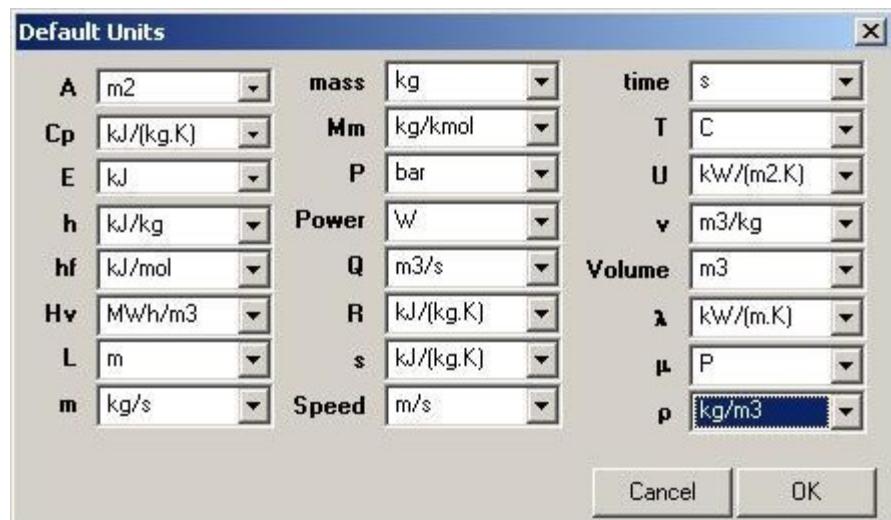
Once you receive your registration key from us, you run the program “**Register.exe**” one more time. You select the application you would like to register, type (or cut and paste) the registration key and click on the button “**Register Now!**”. If all is good, the software will show a dialog box with message “**Successful Registration!**”. Press “OK” and continue.

If there is more than one application to register, you can repeat the same procedure again.

At the end, do not forget to click the button “Save and Exit.”

## Unit Selection

Thermo Utilities supports a large number of units for inputs and outputs. Run the program "C:\THERMOXL\SetUnit.exe" before you start your calculations. Select your desired units. In case you are running "SetUnit.exe" while Excel is running, you need to restart Excel to force it to use newly selected units. Below here you will see a screenshot of "SetUnit.exe".



The unit conversion will apply to both inputs and outputs. If you activate "UNIT.XLA", you can use the strings for the current unit in your worksheet, which improves the readability and security of your calculations. It should be mentioned that Cv, specific heat capacity at constant volume has the same unit as Cp. Steam quality or dryness fraction and Gamma are dimensionless parameters.

## **How to Activate Functions for MS Excel 2010**

In order to activate steam/water functions in MS Excel perform the following procedure:

1. Start your Excel program
2. Click on "File" and Select "Options", a new dialog box called "Excel Options" will open.
3. In the dialog box click on "Add-Ins" on the left side of the window.
4. Make sure the option in front "Manage" points to "Excel Add-ins".
5. Click on the button "Go ...". A new dialog box will open.

Then browse and select C:\THERMOXL\STMXL.XLA

For air and flue gas functions browse and select C:\THERMOXL\AIRXL.XLA

For Lee-Kesler method functions browse and select C:\THERMOXL\LKXL.XLA

For unit conversion function browse and select C:\THERMOXL\UNIT.XLA

You can deactivate any of these groups of functions by deselecting them.

## **How to Activate Functions for MS Excel 2007**

In order to activate steam/water functions in MS Excel perform the following procedure:

1. Start your Excel program
2. Click the Microsoft Office Button , and then click Excel "Options".
3. Click the Add-Ins category.
4. In the "Manage" box, click "Excel Add-ins", and then click "Go ...".

Then browse and select C:\THERMOXL\STMXL.XLA

For air and flue gas functions browse and select C:\THERMOXL\AIRXL.XLA

For Lee-Kesler method functions browse and select C:\THERMOXL\LKXL.XLA

For unit conversion function browse and select C:\THERMOXL\UNIT.XLA

You can deactivate any of these groups of functions by deselecting them.

## **How to Activate Functions for MS Excel 97-2003**

In order to activate steam/water functions in MS Excel perform the following procedure:

1. Start your Excel program
2. Select "Tool"
3. Select "Add-ins"

Then browse C:\THERMOXL\STMXML.XLA

For air and flue gas functions browse and select C:\THERMOXL\AIRXL.XLA

For Lee-Kesler method functions browse and select C:\THERMOXL\LKXL.XLA

For unit conversion function browse and select C:\THERMOXL\UNIT.XLA

You can deactivate any of these groups of functions by deselecting them.

## List of Functions for properties of steam/water

When you activate STMXL.XLA, you have access to all steam/water functions. By clicking on



button in MS Excel a dialog over all function comes up. Select "**User Defined**" and you will have a list over all user defined functions. When you pick a function, a brief description of the function appears at the bottom of the dialog box. If you press "Next", Excel will continue with a dialog box that asks for the necessary inputs for the function. In case, you press "Enter" button, you should fill all the parameters with numbers, cell reference, variable's name and so on. These are the normal Excel functions behavior and are not specific for this program. If you need more help please see the on-line help of MS Excel or the user manual. The function names are compatible with the DLL version of the software. User who upgrade to this version from DLL version, will find several new functions. There are some simple rules that will help you to remember functions' names. Here, you have a complete list of functions for properties of steam and water:

Function	Description	Comment
STMCp	(P,T)-->Cp, Heat capacity	Returns 0 in demo version.
STMCpSS	(P)-->Cp for saturated steam	Returns 0 in demo version.
STMCpSW	(P)-->Cp for saturated water	Returns 0 in demo version.
STMDv	(V,T)-->Dv, Dynamic viscosity	Returns 0 in demo version.
STMPHQ	(P,H)-->Q, Dryness fraction	Returns 0 in demo version.
STMPHS	(P,H)-->S, Specific entropy	Returns 0 in demo version.
STMPHT	(P,H)-->T, Temperature	Returns 0 in demo version.
STMPHV	(P,H)-->V, Specific volume	Returns 0 in demo version.
STMPQH	(P,Q)-->H, Specific enthalpy	Returns 0 in demo version.
STMPQS	(P,Q)-->S, Specific entropy	Returns 0 in demo version.
STMPQV	(P,Q)-->V, Specific volume	Returns 0 in demo version.
STMPSH	(P,S)-->H, Specific enthalpy	Returns 0 in demo version.
STMPSQ	(P,S)-->Q, Dryness fraction	Returns 0 in demo version.
STMPST	(P,S)-->T, Temperature	Returns 0 in demo version.
STMPSV	(P,S)-->V, Specific volume	Returns 0 in demo version.
<b>STMPT</b>	<b>(P)--&gt;T, Saturation temperature</b>	<b>Should work in demo version.</b>
STMPTH	(P,T)-->H, Specific enthalpy	Returns 0 in demo version.
STMPTS	(P,T)-->S, Specific entropy	Returns 0 in demo version.
STMPTV	(P,T)-->V, Specific volume	Returns 0 in demo version.
STMPVH	(P,V)-->H, Specific enthalpy	Returns 0 in demo version.
STMPVQ	(P,V)-->Q, Dryness fraction	Returns 0 in demo version.
STMPVS	(P,V)-->S, Specific entropy	Returns 0 in demo version.
STMPVT	(P,V)-->T, Temperature	Returns 0 in demo version.
STMTc	(V,T)-->Tc, Thermal conductivity	Returns 0 in demo version.
<b>STMTP</b>	<b>(T)--&gt;P, Saturation pressure</b>	<b>Should work in demo version.</b>
STMTQH	(T,Q)-->H, Specific enthalpy	Returns 0 in demo version.
STMTQS	(T,Q)-->S, Specific entropy	Returns 0 in demo version.
STMTQV	(T,Q)-->V, Specific volume	Returns 0 in demo version.

## List of Functions for Properties of Air/Flue Gases

Functions for properties of air/flue gases are based on equations accepted by ASHRAE and are compatible with formulations accepted by CIBSE (Chartered Institute of Building Services Engineers). When you activate AIRXL.XLA, you have access to all air/flue gases functions. By clicking on



button in MS Excel a dialog over all function comes up. Select "**User Defined**" and you will have a list over all user defined functions. When you pick a function, a brief description of the function appears at the bottom of the dialog box. If you press "Next", Excel will continue with a dialog box that asks for the necessary inputs for the function. In case, you press "Enter" button, you should fill all the parameters with numbers, cell reference, variable's name and so on. These are the normal Excel functions behavior and are not specific for this program. If you need more help please see the on-line help of MS Excel or the user manual. The function names are compatible with the DLL version of the software. User who upgrade to this version from DLL version, will find several new functions. There are some simple rules that will help you to remember functions' names. Here, you have a complete list of functions for properties of Air and Exhaust Gas:

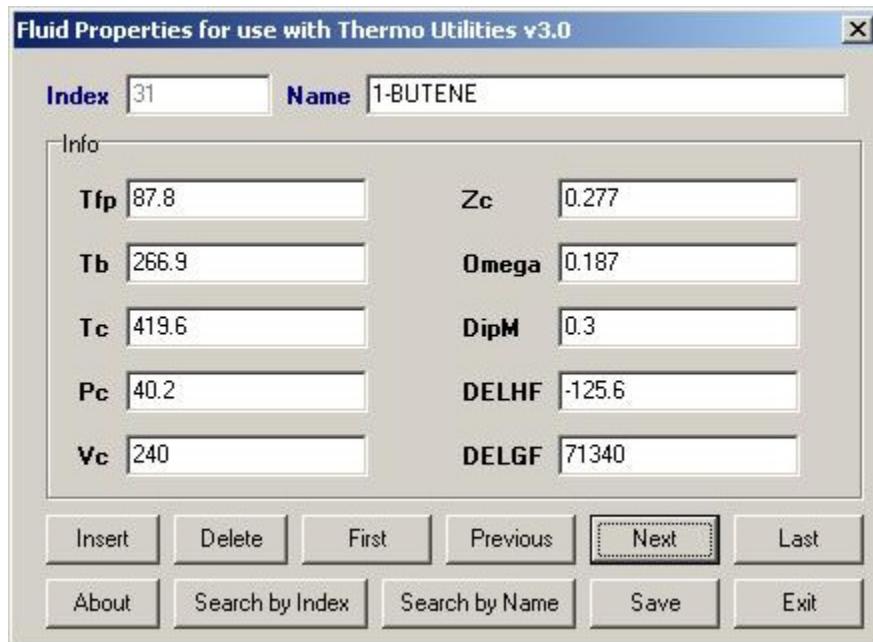
Function	Description	Comment
AirCpT	(mc,Cp)-->T, Temperature	Returns 0 in demo version.
AirDpt	(mc,P)--> Dpt, Dew point temperature	Returns 0 in demo version.
AirDv	(mc,P,T)-->Dv, Dynamic viscosity	Returns 0 in demo version.
<b>AirGC</b>	<b>(mc)--&gt;Gc, Gas constant</b>	<b>Should work in demo version.</b>
AirHT	(mc,H)-->T, Temperature	Returns 0 in demo version.
<b>AirMM</b>	<b>(mc)--&gt;Mm, Molecular mass</b>	<b>Should work in demo version.</b>
AirST	(mc,S)-->T, Temperature	Returns 0 in demo version.
AirTc	(mc,P,T)-->Tc, Thermal conductivity	Returns 0 in demo version.
AirTCp	(mc,T)-->Cp, Heat capacity at constant P	Returns 0 in demo version.
AirTCv	(mc,T)-->Cv, Heat capacity at constant V	Returns 0 in demo version.
AirTGamma	(mc,T)-->Gamma = Cp/Cv	Returns 0 in demo version.
AirTH	(mc,T)-->H, Specific enthalpy	Returns 0 in demo version.
AirTS	(mc,T)-->S, Specific entropy	Returns 0 in demo version.
FlueCpT	(Cp,%)-->T, Temperature	Returns 0 in demo version.
FlueDpt	(P,%)--> Dpt, Dew point temperature	Returns 0 in demo version.
FlueDv	(P,T,%)-->Dv, Dynamic viscosity	Returns 0 in demo version.
<b>FlueGC</b>	<b>(%)--&gt;Gc, Gas constant</b>	<b>Should work in demo version.</b>
FlueHT	(H,%)-->T, Temperature	Returns 0 in demo version.
<b>FlueMM</b>	<b>(%)--&gt;Mm, Molecular mass</b>	<b>Should work in demo version.</b>
FlueST	(S,%)-->T, Temperature	Returns 0 in demo version.
FlueTc	(P,T,%)-->Tc, Thermal conductivity	Returns 0 in demo version.
FlueTCp	(T,%)-->Cp, Heat capacity at constant P	Returns 0 in demo version.
FlueTCv	(T,%)-->Cv, Heat capacity at constant V	Returns 0 in demo version.
FlueTGamma	(T,%)-->Gamma = Cp/Cv	Returns 0 in demo version.
FlueTH	(T,%)-->H, Specific enthalpy	Returns 0 in demo version.
FlueTS	(T,%)-->S, Specific entropy	Returns 0 in demo version.
<b>GasDensity</b>	<b>(P,T,Gc)--&gt;Density</b>	<b>Should work in demo version.</b>
<b>GasS</b>	<b>(P,Gc,Satm)--&gt;S at pressure, P</b>	<b>Should work in demo version.</b>
<b>GasSAtm</b>	<b>(P,Gc,S)--&gt;Satm = S at atmospheric pressure</b>	<b>Should work in demo version.</b>
ScreenPS	(DBT,WBT)-->PS, Percentage saturation	Returns 0 in demo version.
ScreenRH	(DBT,WBT)-->RH, Relative humidity	Returns 0 in demo version.
ScreenSH	(DBT,WBT)-->SH, Specific humidity	Returns 0 in demo version.
ScreenVWR	(DBT,WBT)-->VWR, Volumetric water ratio	Returns 0 in demo version.
SlingPS	(DBT,WBT)-->PS, Percentage saturation	Returns 0 in demo version.
SlingRH	(DBT,WBT)-->RH, Relative humidity	Returns 0 in demo version.
SlingSH	(DBT,WBT)-->SH, Specific humidity	Returns 0 in demo version.
SlingVWR	(DBT,WBT)-->VWR, Volumetric water ratio	Returns 0 in demo version.

## Fluid Properties Utility for Use with Lee-Kesler Method

The current version of Lee-Kesler method support 467 different chemical compounds. You can use the utility software "C:\THERMOXL\fluidpro.exe" to view, edit or add new entries to our database. When you edit or add new entries, you should use the units mentioned in ellipses below. The database supports the following:

- Normal freezing point (T<sub>fp</sub>, K)
- Normal boiling point (T<sub>b</sub>, K at 1 atmosphere)
- Critical temperature (T<sub>c</sub>, K)
- Critical pressure (P<sub>c</sub>, bar)
- Critical specific volume (V<sub>c</sub>, cm<sup>3</sup>/mol)
- Critical compressibility factor (Z<sub>c</sub>, no dimension)
- Pitzer's acentric factor (Omega, no dimension)
- Dipole moment (DipM, debyes)
- Standard enthalpy of formation (DELHF, J/mol)
- Standard Gibbs energy of formation (DELGF, J/mol)

Here is a screenshot of "fluidpro.exe".



## List of Functions for Lee-Kesler method

These functions compute the thermodynamic properties of chemicals by using reduced pressure and temperature. When you activate LKXL.XLA, you have access to these functions. By clicking on

*fx*

button in MS Excel a dialog over all function comes up. Select "**User Defined**" and you will have a list over all user defined functions. When you pick a function, a brief description of the function appears at the bottom of the dialog box. If you press "Next", Excel will continue with a dialog box that asks for the necessary inputs for the function. In case, you press "Enter" button, you should fill all the parameters with numbers, cell reference, variable's name and so on. These are the normal Excel functions behavior and are not specific for this program. If you need more help please see the on-line help of MS Excel or the user manual. The function names are compatible with the DLL version of the software. User who upgrade to this version from DLL version, will find several new functions. There are some simple rules that will help you to remember functions' names. Here is the complete list of functions:

Function	Description	Comment
LKPFT	(P,F)->T, reduced temperature	Returns 0 in demo version.
LKPHT	(P,H)->T, reduced temperature	Returns 0 in demo version.
LKPQF	(P,Q)->F, fugacity-pressure ratio	Returns 0 in demo version.
LKPQH	(P,Q)->H, residual enthalpy	Returns 0 in demo version.
LKPQS	(P,Q)->S, residual entropy	Returns 0 in demo version.
LKPQZ	(P,Q)->Z, compressibility factor	Returns 0 in demo version.
LKPST	(P,S)->T, reduced temperature	Returns 0 in demo version.
LKPZT	(P,Z)->T, reduced temperature	Returns 0 in demo version.
<b>LKPT</b>	<b>(P)-&gt;T, reduced saturation temperature</b>	<b>Should work in demo version.</b>
LKPTF	(P,T)->F, fugacity-pressure ratio	Returns 0 in demo version.
LKPTH	(P,T)->H, residual enthalpy	Returns 0 in demo version.
LKPTS	(P,T)->S, residual entropy	Returns 0 in demo version.
LKPTZ	(P,T)->Z, compressibility factor	Returns 0 in demo version.
LKTP	(T)->P, reduced saturation pressure	Returns 0 in demo version.
LKTQF	(T,Q)->F, fugacity-pressure ratio	Returns 0 in demo version.
LKTQH	(T,Q)->H, residual enthalpy	Returns 0 in demo version.
LKTQS	(T,Q)->S, residual entropy	Returns 0 in demo version.
LKTQZ	(T,Q)->Z, compressibility factor	Returns 0 in demo version.

## **Simple Rules to Remember Functions' Names**

All functions for steam/water properties start with **STM** then follow abbreviations for inputs needed and at last the output. Some examples are **STMPTH** needs **P**, pressure and **T**, temperature to calculate **H**, specific enthalpy, **STMPHT** needs **P**, pressure and **H**, specific enthalpy and calculates **T**, temperature.

The same rule applies to functions for dry air, moist air and flue gases. Functions for dry and moist air start with **Air** and functions for flue gases start with **Flue**. All functions for dry/moist air need **mc**, moisture content. Therefore it has been omitted from the function's name. The same is with the flue gas functions. All of them require the volumetric or mole fraction of the gases. Functions for screen hygrometer start with **Screen** and functions for sling hygrometer start with **Sling**. These functions calculate **SH**, specific humidity, **RH**, relative humidity, **PS**, percentage saturation and **VWR**, volumetric water ratio.

The Lee-Kesler method functions start with **LK** then follow abbreviations for inputs needed and at last the output. All these functions need Pitzer's acentric factor as the last input. Some examples are **LKPTH** needs **P**, reduced pressure and **T**, reduced temperature and also acentric factor to calculate **H**, residual specific enthalpy, **LKPHT** needs **P**, reduced pressure and **H**, residual specific enthalpy, acentric factor and calculates **T**, reduced temperature.

## **Abbreviations Used for Function Names and Input/ Output Parameters**

- Cp: Specific heat capacity at constant pressure
- Cv: Specific heat capacity at constant volume
- Dv: Dynamic viscosity
- F: Fugacity-pressure ratio
- Gamma: Ratio of Cp/Cv
- GC: Gas constant
- H: Specific enthalpy (residual specific enthalpy for Lee-Kesler method)
- mc: Moisture content
- MM: Molecular mass
- P: Pressure (reduced pressure for Lee-Kesler method)
- PS: Percentage saturation
- Q: Steam quality = dryness fraction = 1 - wetness fraction
- RH: Relative humidity
- S: Specific entropy (residual specific entropy for Lee-Kesler method)
- SH: Specific humidity = moisture content
- T: Temperature (reduced temperature in Lee-Kesler method)
- Tc: Thermal conductivity
- V: Specific volume
- VWR: Volumetric water ratio
- Z: Compressibility factor

## **Macro Development and Error Handling**

You can view our function prototypes and VBA interface by selecting "Tool", "Macro", "Visual Basic Editor" (short cut ALT+F11). By developing your own macros you can speed up your calculations and also make your own dialog boxes for input/output. This is particularly true when you need several outputs with the same set of inputs.

### **Error handling/reporting for Steam/water functions**

All functions return large negative numbers in case of error. No function returns a negative number less than **-1000** no matter what units are used. The returned values and reasons are:

- -1001: The pressure is outside the acceptable range specified in IFC formulation for Industrial use!

$0.01 \text{ bar} < P < 1000 \text{ bar}$

- -1002: The temperature is outside the acceptable range specified in IFC formulation for Industrial use!

$0 \text{ C} < T < 800 \text{ C}$

- -1003: Dryness fraction should be within the following limits:

$0.0 = Q \leq 1.0$

- -1004: Pressure of the wet steam may not be more than 221.0 bar (pressure at critical point is 221.2 bar) i.e.

$P \leq 221.0 \text{ bar}$

- -1005: Temperature of the wet steam may not be more than 374.0 C (temperature at critical point is 374.15 C) i.e.

$T \leq 374.0 \text{ C}$

- -1012: It is impossible to find a point with the specified pressure [P] and specific entropy [s]!
- -1013: It is impossible to find a point with the specified pressure [P] and specific volume [v]!
- -1014: It is impossible to find a point with the specified pressure [P] and specific enthalpy [h]!
- -1015: Inputs are not enough to determine the state of the steam or water. Pressure and temperature are too close to wet steam data.
- -1016: Pressure and temperature are too close to critical point.
- -1017: Specific volume is too small.

## **Error Handling/Reporting for Air and Flue Gas Functions**

All functions return large negative numbers in case of error. No function returns a negative number less than **-20E+9** no matter what units are used. The returned values and reasons are:

- -21E+9: Moisture content, mc, is not acceptable!

$0 \leq mc < 0.30$

- -22E+9: Volumetric compositions should be within the interval zero and one and the sum must be one.
- -23E+9: Temperature should be within the following limits:

$-40 \text{ C} < T < 1500 \text{ C}$

- -24E+9: It is impossible to find a temperature with the specified specific enthalpy.
- -25E+9: It is impossible to find a temperature with the specified specific entropy.
- -26E+9: It is impossible to find a temperature with the specified specific heat capacity.
- -27E+9: The wet bulb temperature is limited to:

$-40 \text{ C} < T < 70 \text{ C}$

- -28E+9: The following condition should be satisfied:

$\text{DryBulbT} \geq \text{WetBulbT}$

- -29E+9: The set of values for dry and wet bulb temperatures are not possible!
- -30E+9: Pressure is outside the acceptable range:

1.  $1 \text{ bar} < P < 20 \text{ bar}$

- -31E+9: Gas constant is too small.

## Error Handling/Reporting for Lee-Kesler Functions

All functions return large negative numbers in case of error. No function returns a negative number less than -2000. No matter what units are used. The returned values and reasons are:

- -2001: The pressure is outside the acceptable range!

$$0.01 < \text{Pr} < 10$$

$\text{Pr}$  = Reduced pressure =  $P/P_{\text{cr}}$

$P_{\text{cr}}$  = Critical pressure

$P$  = Pressure

- -2002: The temperature is outside the acceptable range!

$$0.3 < \text{Tr} < 4.0$$

$\text{Tr}$  = Reduced temperature =  $T/T_{\text{cr}}$

$T_{\text{cr}}$  = Critical temperature

$T$  = Temperature

- -2003: Dryness fraction should be within the following limits:

$$0.0 \leq Q \leq 1.0$$

- -2004: Pressure of wet vapor may not be more than  $P_{\text{cr}}$  i.e.

$$\text{Pr} \leq 1.0$$

- -2005: Temperature of wet vapor may not be more than  $T_{\text{cr}}$  i.e.

$$\text{Tr} \leq 1.0$$

- -2012: It is impossible to find a point with the specified reduced pressure [Pr] and reduced specified entropy [sr]!
- -2013: It is impossible to find a point with the specified reduced pressure [Pr] and compressibility factor [Z]!

$$Z = (V * P) / (R * T)$$

$V$  = Specific volume

$$R = \text{Gas Constant} = 8.3144 \text{ J/(mol.K)} = 10.732 \text{ psia.ft}^2/(\text{lb-mol.R})$$

- -2014: It is impossible to find a point with the specified reduced pressure [Pr] and reduced specific enthalpy [h]!
- -2015: Inputs are not enough to determine the state of the fluid. Pressure and temperature are too close to wet vapor data.
- -2016: It is impossible to find a point with the specified reduced pressure [Pr] and reduced fugacity-pressure ratio [f]!
- -2020: Acentric factor is out of acceptable range.

$$-0.5 < Af < 2.0$$

## **VBA Function Prototypes for Steam and Water Properties**

You can view the content of “STMXL.XLA” by using short cut ALT+F11. The function prototypes are:

```
Private Declare Sub VBASATP Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByRef T#, ByRef vf#, ByRef vg#,
ByRef hf#, ByRef hg#, ByRef sf#, ByRef sg#, ByRef ErrorCode%)
```

```
Private Declare Sub VBASATT Lib "C:\THERMOXL\TUXL.DLL" (ByVal T#, ByRef P#, ByRef vf#, ByRef vg#,
ByRef hf#, ByRef hg#, ByRef sf#, ByRef sg#, ByRef ErrorCode%)
```

```
Private Declare Sub VBASUPERHEATED Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal T#, ByRef V#,
ByRef H#, ByRef S#, ByRef Q#, ByRef ErrorCode%)
```

```
Private Declare Sub VBAPS Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal S#, ByRef T#, ByRef V#,
ByRef H#, ByRef Q#, ByRef ErrorCode%)
```

```
Private Declare Sub VBAPH Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal H#, ByRef T#, ByRef V#,
ByRef S#, ByRef Q#, ByRef ErrorCode%)
```

```
Private Declare Sub VBAPV Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal V#, ByRef T#, ByRef H#,
ByRef S#, ByRef Q#, ByRef ErrorCode%)
```

```
Private Declare Sub CONDUCTIVITY Lib "C:\THERMOXL\TUXL.DLL" (ByVal V#, ByVal T#, ByRef L#,
ByRef ErrorCode%)
```

```
Private Declare Sub VISCOSITY Lib "C:\THERMOXL\TUXL.DLL" (ByVal V#, ByVal T#, ByRef mi#, ByRef
ErrorCode%)
```

```
Private Declare Sub VBACP Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal T#, ByRef Cp#, ByRef
ErrorCode%)
```

```
Private Declare Sub VBACP_T0 Lib "C:\THERMOXL\TUXL.DLL" (ByVal T#, ByRef Cp#, ByRef ErrorCode%)
```

```
Private Declare Sub VBACP_T1 Lib "C:\THERMOXL\TUXL.DLL" (ByVal T#, ByRef Cp#, ByRef ErrorCode%)
```

```
Private Declare Sub STATEOFREGSTM Lib "C:\THERMOXL\TUXL.DLL" (ByRef State%)
```

## **VBA Function Prototypes for Air and Flue Gas Properties**

You can view the content of “AIRXL.XLA” by using short cut ALT+F11. The function prototypes are:

```
Private Declare Sub VBAEGGC Lib "C:\THERMOXL\TUXL.DLL" (ByVal N2#, ByVal O2#, ByVal CO2#, ByVal Ar#, ByVal H2O#, ByVal SO2#, ByRef GC#, ByRef ErrorCode%)
```

```
Private Declare Sub VBAEGMM Lib "C:\THERMOXL\TUXL.DLL" (ByVal N2#, ByVal O2#, ByVal CO2#, ByVal Ar#, ByVal H2O#, ByVal SO2#, ByRef MM#, ByRef ErrorCode%)
```

```
Private Declare Sub VBAEGT Lib "C:\THERMOXL\TUXL.DLL" (ByVal N2#, ByVal O2#, ByVal CO2#, ByVal Ar#, ByVal H2O#, ByVal SO2#, ByVal T#, ByRef H#, ByRef Cp#, ByRef Cv#, ByRef Gam#, ByRef S#, ByRef ErrorCode%)
```

```
Private Declare Sub VBAEGHT Lib "C:\THERMOXL\TUXL.DLL" (ByVal N2#, ByVal O2#, ByVal CO2#, ByVal Ar#, ByVal H2O#, ByVal SO2#, ByVal H#, ByRef T#, ByRef ErrorCode%)
```

```
Private Declare Sub VBAEGST Lib "C:\THERMOXL\TUXL.DLL" (ByVal N2#, ByVal O2#, ByVal CO2#, ByVal Ar#, ByVal H2O#, ByVal SO2#, ByVal S#, ByRef T#, ByRef ErrorCode%)
```

```
Private Declare Sub VBAEGCPT Lib "C:\THERMOXL\TUXL.DLL" (ByVal N2#, ByVal O2#, ByVal CO2#, ByVal Ar#, ByVal H2O#, ByVal SO2#, ByVal Cp#, ByRef T#, ByRef ErrorCode%)
```

```
Private Declare Sub VBAEGTC Lib "C:\THERMOXL\TUXL.DLL" (ByVal N2#, ByVal O2#, ByVal CO2#, ByVal Ar#, ByVal H2O#, ByVal SO2#, ByVal T#, ByVal P#, ByRef Tc#, ByRef ErrorCode%)
```

```
Private Declare Sub VBAEGDV Lib "C:\THERMOXL\TUXL.DLL" (ByVal N2#, ByVal O2#, ByVal CO2#, ByVal Ar#, ByVal H2O#, ByVal SO2#, ByVal T#, ByVal P#, ByRef Dv#, ByRef ErrorCode%)
```

```
Private Declare Sub VBAEGDPT Lib "C:\THERMOXL\TUXL.DLL" (ByVal N2#, ByVal O2#, ByVal CO2#, ByVal Ar#, ByVal H2O#, ByVal SO2#, ByVal P#, ByRef Dpt#, ByRef ErrorCode%)
```

```
Private Declare Sub VBASLINGSH Lib "C:\THERMOXL\TUXL.DLL" (ByVal DryBulbT#, ByVal WetBulbT#, ByRef SH#, ByRef ErrorCode%)
```

```
Private Declare Sub VBASLINGPS Lib "C:\THERMOXL\TUXL.DLL" (ByVal DryBulbT#, ByVal WetBulbT#, ByRef PS#, ByRef ErrorCode%)
```

```
Private Declare Sub VBASLINGRH Lib "C:\THERMOXL\TUXL.DLL" (ByVal DryBulbT#, ByVal WetBulbT#, ByRef RH#, ByRef ErrorCode%)
```

```
Private Declare Sub VBASLINGVWR Lib "C:\THERMOXL\TUXL.DLL" (ByVal DryBulbT#, ByVal WetBulbT#, ByRef VWR#, ByRef ErrorCode%)
```

```
Private Declare Sub VBASCREENSH Lib "C:\THERMOXL\TUXL.DLL" (ByVal DryBulbT#, ByVal WetBulbT#, ByRef SH#, ByRef ErrorCode%)
```

```
Private Declare Sub VBASCREENPS Lib "C:\THERMOXL\TUXL.DLL" (ByVal DryBulbT#, ByVal WetBulbT#, ByRef PS#, ByRef ErrorCode%)
```

*Private Declare Sub VBASCREENRH Lib "C:\THERMOXL\TUXL.DLL" (ByVal DryBulbT#, ByVal WetBulbT#,  
ByRef RH#, ByRef ErrorCode%)*

*Private Declare Sub VBASCREENVWR Lib "C:\THERMOXL\TUXL.DLL" (ByVal DryBulbT#, ByVal WetBulbT#,  
ByRef VWR#, ByRef ErrorCode%)*

*Private Declare Sub VBAAIRGC Lib "C:\THERMOXL\TUXL.DLL" (ByVal mc#, ByRef GC#, ByRef ErrorCode%)*

*Private Declare Sub VBAIRMM Lib "C:\THERMOXL\TUXL.DLL" (ByVal mc#, ByRef MM#, ByRef ErrorCode%)*

*Private Declare Sub VBAAIRT Lib "C:\THERMOXL\TUXL.DLL" (ByVal mc#, ByVal T#, ByRef H#, ByRef Cp#,  
ByRef Cv#, ByRef Gam#, ByRef S#, ByRef ErrorCode%)*

*Private Declare Sub VBAAIRHT Lib "C:\THERMOXL\TUXL.DLL" (ByVal mc#, ByVal H#, ByRef T#, ByRef  
ErrorCode%)*

*Private Declare Sub VBAIRCPT Lib "C:\THERMOXL\TUXL.DLL" (ByVal mc#, ByVal Cp#, ByRef T#, ByRef  
ErrorCode%)*

*Private Declare Sub VBAIRST Lib "C:\THERMOXL\TUXL.DLL" (ByVal mc#, ByVal S#, ByRef T#, ByRef  
ErrorCode%)*

*Private Declare Sub VAAIRTC Lib "C:\THERMOXL\TUXL.DLL" (ByVal mc#, ByVal T#, ByVal P#, ByRef Tc#,  
ByRef ErrorCode%)*

*Private Declare Sub VAAIRDV Lib "C:\THERMOXL\TUXL.DLL" (ByVal mc#, ByVal T#, ByVal P#, ByRef Dv#,  
ByRef ErrorCode%)*

*Private Declare Sub VAAIRDPT Lib "C:\THERMOXL\TUXL.DLL" (ByVal mc#, ByVal P#, ByRef Dpt#, ByRef  
ErrorCode%)*

*Private Declare Sub VBADENSITY Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal GC#, ByVal T#, ByRef  
Ro#, ByRef ErrorCode%)*

*Private Declare Sub VBAADJUSTS Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal GC#, ByVal S#, ByRef  
S0#, ByRef ErrorCode%)*

*Private Declare Sub VBAADJUSTS0 Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal GC#, ByVal S0#, ByRef  
S#, ByRef ErrorCode%)*

*Private Declare Sub STATEOFREGAIR Lib "C:\THERMOXL\TUXL.DLL" (ByRef State%)*

## **VBA Function Prototypes for Lee-Kesler Method**

You can view the content of “LKXL.XLA” by using short cut ALT+F11. The function prototypes are:

```
Private Declare Sub LEKEPHT Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal H#, ByVal Omega#, ByRef T#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKEPST Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal S#, ByVal Omega#, ByRef T#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKEPFT Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal F#, ByVal Omega#, ByRef T#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKEPZT Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal Z#, ByVal Omega#, ByVal  
SolutionIndex%, ByRef T#, ByRef ErrorCode%)
```

```
Private Declare Sub LEKEPTZ Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal T#, ByVal Omega#, ByRef Z#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKEPQZ Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal Q#, ByVal Omega#, ByRef Z#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKETQZ Lib "C:\THERMOXL\TUXL.DLL" (ByVal T#, ByVal Q#, ByVal Omega#, ByRef Z#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKEPTH Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal T#, ByVal Omega#, ByRef H#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKEPQH Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal Q#, ByVal Omega#, ByRef  
H#, ByRef ErrorCode%)
```

```
Private Declare Sub LEKETQH Lib "C:\THERMOXL\TUXL.DLL" (ByVal T#, ByVal Q#, ByVal Omega#, ByRef H#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKEPTS Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal T#, ByVal Omega#, ByRef S#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKEPQS Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal Q#, ByVal Omega#, ByRef S#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKETQS Lib "C:\THERMOXL\TUXL.DLL" (ByVal T#, ByVal Q#, ByVal Omega#, ByRef S#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKEPTF Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal T#, ByVal Omega#, ByRef F#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKEPQF Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal Q#, ByVal Omega#, ByRef F#,  
ByRef ErrorCode%)
```

```
Private Declare Sub LEKETQF Lib "C:\THERMOXL\TUXL.DLL" (ByVal T#, ByVal Q#, ByVal Omega#, ByRef F#,  
ByRef ErrorCode%)
```

*Private Declare Sub LEKEPT Lib "C:\THERMOXL\TUXL.DLL" (ByVal P#, ByVal Omega#, ByRef Tsat#, ByRef ErrorCode%)*

*Private Declare Sub LEKETP Lib "C:\THERMOXL\TUXL.DLL" (ByVal T#, ByVal Omega#, ByRef Psat#, ByRef ErrorCode%)*

*Private Declare Sub STATEOFREGLK Lib "C:\THERMOXL\TUXL.DLL" (ByRef State%)*

## List of Worksheets with Function Calls

You should be able to open these files on all MS Excel versions from 97 and higher. The files are located in folder “C:\THERMOXL”

File Location	Brief Description
EXAMPLE-main.xls	How to Activate different add-ins
EXAMPLE-Air and Flue Gas Properties.xls	List of all functions, including 7 demo functions.
EXAMPLE-Steam and Water Properties.xls	List of all functions, including 2 demo functions.
EXAMPLE-LeeKesler.xls	List of all functions, including 1 demo functions.
Example - Unit Conversion.xls	How to obtain the text string for used units.
Chemical Compound Properties.xls	Free data base for 467 different chemicals with information about, normal freezing point, normal boiling point, critical temperature, critical pressure, critical specific volume, critical compressibility factor, Pitzer's acentric factor, dipole moment, standard enthalpy of formation, standard Gibbs energy of formation. <i>Attention! Please verify the information in this file with a second source for important applications.</i>

After activation of different add-ins, you should be able to use the demo functions in each worksheet without any problems. The other functions should return zero.

“Example - Unit Conversion.xls” and “Chemical Compound Properties.xls” should be fully functional.

## Sample Files

### Adiabatic Humidification with Air Washer.xls

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix A.

### Adiabatic Saturation Temperature of Air.xls

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. In order to calculate the adiabatic saturation temperature you need to make an assumption for the value of cell **B38** and use Excel “Goal Seek” to change this value till the value of **B46** is zero.

Goal Seek (Excel 2010): In order to reach “Goal Seek”, first click on “Data” tab. Then click on “What-If Analysis” and last select “Goal Seek ...”. “Goal seek is supported under Excel 97-2003 and later versions.

The screenshot shows an Excel spreadsheet titled "Adiabatic Saturation Temperature of Air.xls". The spreadsheet contains a table of air properties with columns for Dry-bulb temperature (Td), Wet-bulb temperature (Tw), and Atmospheric pressure. Row 38 is highlighted in yellow and contains the formula "temperature Tsat, is 30 degC". The "Goal Seek" dialog box is open over this row, with the "Set cell:" field set to "\$B\$46", the "To value:" field set to 0, and the "By changing cell:" field set to "\$B\$38". The dialog box has "OK" and "Cancel" buttons. The table rows are numbered from 29 to 47. Rows 33 through 47 are labeled "Outputs". Row 46 is labeled "Goal". The column headers are "A" and "B". The "Td" column values are 22.0, 14.0, 1.013, etc. The "Tw" column values are 0.0066, 1.0102, 38.7, etc. The "Assumed" column indicates that the value in row 38 was assumed to be 30.0. The "Goal" column indicates that the value in row 46 was 61.2746.

A	B
Dry-bulb temperature = T1 = Td	22.0
Wet-bulb temperature	14.0
Atmospheric pressure	1.013
Outputs	
Moisture content = g1 = InletMC	0.0066
Spec. heat capacity at inlet = Cp	1.0102
Spec. enthalpy at inlet = InletH	38.7
Assume that adiabatic saturation	
temperature Tsat, is 30 degC	30.0
Saturated air has the same temp.	
for dry and wet bulb which results	
into the following	
moisture content at outlet=OutletMC	0.0272
Now the enthalpy at outlet can be	kg/kg
calculated. OutletH is:	100.0
We know that in an adiabatic	kJ/kg
process diff = OutletH - InletH = 0	61.2746
Now, use the solver to adjust cell	

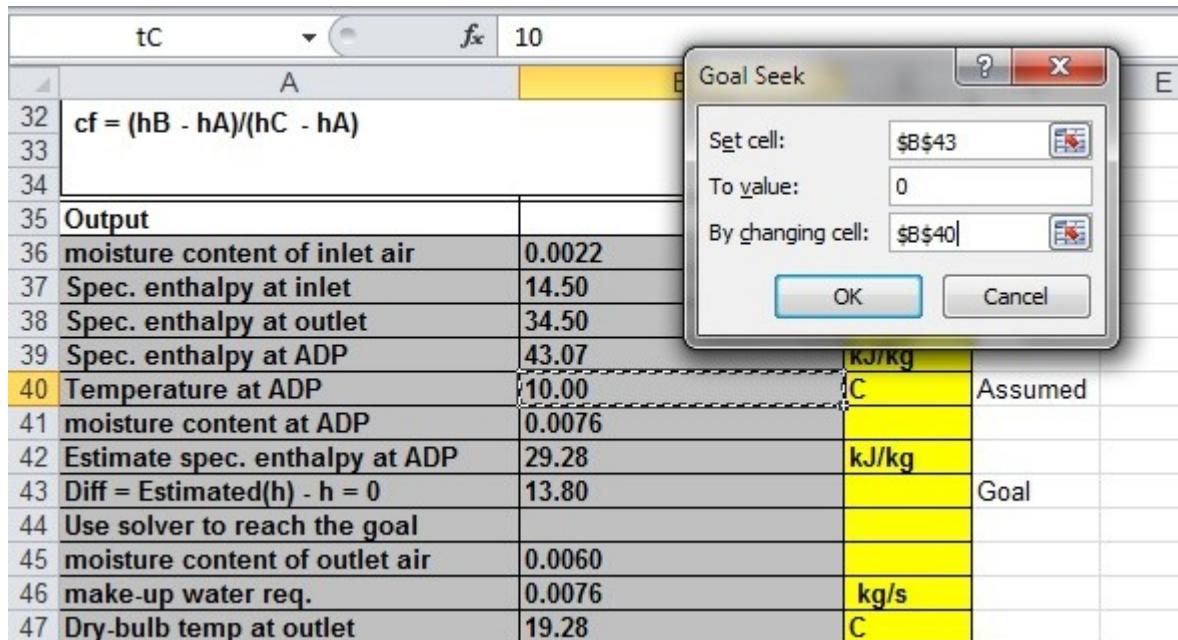
The initial value of B38 was 30C (assumed) and the final value 13.8C. The initial value of B46 was 61.27 kJ/kg and final value 0.

The output of registered version can be seen in Appendix B.

## Air Washer with Heating of Spray Water.xls

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. In order to calculate the apparatus dew-point (ADP) you need to make and assumption for the value of cell **B40** and use Excel “Goal Seek” to change this value till the value of **B43** is zero.

Goal Seek (Excel 2010): In order to reach “Goal Seek”, first click on “Data” tab. Then click on “What-If Analysis” and last select “Goal Seek ...”. “Goal seek is supported under Excel 97-2003 and later versions.



The screenshot shows an Excel spreadsheet titled "tC" with a formula  $cf = (hB - hA)/(hC - hA)$  in cell A32. Below it is a table of output parameters:

		kJ/kg		
35	Output			
36	moisture content of inlet air	0.0022		
37	Spec. enthalpy at inlet	14.50		
38	Spec. enthalpy at outlet	34.50		
39	Spec. enthalpy at ADP	43.07		
40	Temperature at ADP	10.00	C Assumed	
41	moisture content at ADP	0.0076		
42	Estimate spec. enthalpy at ADP	29.28	kJ/kg	
43	Diff = Estimated(h) - h = 0	13.80		Goal
44	Use solver to reach the goal			
45	moisture content of outlet air	0.0060		
46	make-up water req.	0.0076	kg/s	
47	Dry-bulb temp at outlet	19.28	C	

A "Goal Seek" dialog box is overlaid on the spreadsheet, set to find a value for cell \$B\$43 (0) by changing cell \$B\$40.

The initial value of **B40** was 10C (assumed) and the final value 15.38C. The initial value of **B43** was 13.8 kJ/kg and final value 0.

The output of registered version can be seen in Appendix C.

## Calculating Humid Air Data.xls

Not all the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The output of registered version can be seen in Appendix D.

## **Closed-feed Heater.xls**

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix E.

## **Coal Combustion.xls**

Most outputs calculated in this worksheet do not need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix F.

## **Combustion of Biomass Fuel.xls**

Most outputs calculated in this worksheet do not need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix G.

## **Combustion of Fossil Fuels.xls**

Most outputs calculated in this worksheet do not need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix H.

## **Compression Process Calculations.xls**

This worksheet shows the calculations for a single stage compressor. All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix I.

## **Condenser Design.xls**

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix J.

## **Cooling Tower.xls**

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix K.

## **Direct Steam Injection - Steam Humidifier.xls**

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix L.

## **Expansion Process - Gas Turbine.xls**

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix M.

## **Feed Heater.xls**

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix N.

## **Lkdemo1.xls, Lkdemo2.xls, Lkdemo3.xls, Lkdemo4.xls and Lkdemo5.xls**

These five examples show how Lee-Kesler method can be used. Most of the outputs calculated in these worksheets need a registered version. The files are located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix O1 thru Appendix O5.

## Mixing of Two Air Streams.xls

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix P.

## Pan Steam Humidifier.xls

Most of the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. In order to calculate the ratio of sensible heat to total heat ( $Q_s/Q$ ) you need to make an assumption for the value of cell **B36** and use Excel “Goal Seek” to change this value till the value of **B41** is 0.20.

Goal Seek (Excel 2010): In order to reach “Goal Seek”, first click on “Data” tab. Then click on “What-If Analysis” and last select “Goal Seek ...”. “Goal seek is supported under Excel 97-2003 and later versions.

The screenshot shows a Microsoft Excel spreadsheet titled "Pan Steam Humidifier.xls". The spreadsheet contains several rows of data and formulas. A "Goal Seek" dialog box is overlaid on the spreadsheet, indicating that cell B41 is set to 0.2, changing cell B36, and the target value is 0.2. The spreadsheet includes formulas for calculating steam supplied and moisture content, and specifies units for various parameters like DBT and kJ/kg.

28	U.Z	A	=Qs/Q
29	Load on the humidifier is:		
30	$Q = m_A * (h_B - h_A)$		
31	and the steam supplied by humidifier is:		
32	$m_{Steam} = m_A * (m_c B - m_c A)$		
33			
34	Output		
35	moisture content of inlet air	0.0022	
36	Outlet air, DBT	15.00	C Assumed
37	Spec. enthalpy at inlet	14.5	kJ/kg
38	Spec. enthalpy at outlet	35.3	kJ/kg
39	Load on the humidifier = total heat	41.5448	kW
40	Sensible heat	12.0738	kJ/kg
41	Qs / Q = 0.2	0.2906	Goal
42	Use the solver to reach the goal		
43	steam supplied	0.0117	kg/s

The initial value of **B36** was 15C (assumed) and the final value 12.66C. The initial value of **B41** was 0.29 and final value 0.20.

The output of registered version can be seen in Appendix Q.

## **Pump.xls**

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix R.

## **Regenerative Steam Cycle.xls**

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix S.

## **Sensible Cooling Process.xls**

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix T.

## Sensible Cooling with Dehumidification.xls

Most of the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. Apparatus dew-point moisture content (cell **B39**) should make the calculated value of Eq1 and Eq2 the same or in other words the difference (cell **B44**) should be zero.

Goal Seek (Excel 2010): In order to reach “Goal Seek”, first click on “Data” tab. Then click on “What-If Analysis” and last select “Goal Seek ...”. “Goal seek is supported under Excel 97-2003 and later versions.

A	B	C	D
28 defined by moisture content differences:			
29 $cf = (mcA - mcB)/(mcA - mcC)$			
30 or			
31 $cf = (hA - hB)/(hA - hC)$			
32			
33			
34			
35 Output			
36 Specific enthalpy of the on-coil air	49.4		
37 Specific enthalpy of the off-coil air	32.2385	kJ/kg	
38 Load on the coil	34.4695	kW	
39 Apparatus dew-point moisture content	0.0080		Assumed
40 Apparatus dew-point temperature	10.9	C	
41 Apparatus dew-point enthalpy	31.1	kJ/kg	
42 Coil contact factor Eq1	1.00		
43 Coil contact factor Eq2	0.94		
44 Diff = Eq1-Eq2 = 0	0.0608		Goal
45 Use the solver to reach the goal			
46			

The initial value of **B39** was 0.008 (assumed) and the final value 0.0077. The initial value of **B44** was 0.0608 and final value 0.00.

The output of registered version can be seen in Appendix U.

## Sensible Heating Process.xls

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix V.

## **Steam Turbine.xls**

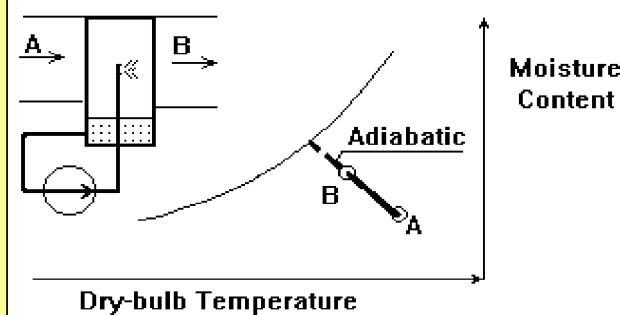
All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix W.

## **Valve - Throttling Process.xls**

All the outputs calculated in this worksheet need a registered version. The file is located in folder “C:\THERMOXL”. The calculations are straight forward. The output of registered version can be seen in Appendix X.

## Appendix A

In an air conditioning plant, air flow rate of 2 kg/s passes through a spray water humidifier with a contact factor 0.7. Determine the moisture content and temperature of the air leaving the humidifier and the amount of make-up water needed. The dry and wet-bulb temperature of the inlet air are 25 C and 15 C respectively.



Inputs		Units
Inlet air, DBT	24.00	C
Inlet air, WBT	15.00	C
Inlet air, mass flow rate	2.00	kg/s
Contact factor of the humidifier	0.70	
Atmospheric pressure	1.01	bar

The contact factor of a humidifier is defined as the efficiency for humidification. A 100% efficient humidifier will bring the moisture content of the air to the saturation moisture content at the apparatus dew-point,  $mcC$ . The contact factor of the humidifier can be defined by the moisture content differences:

$$cf = (mcB - mcA)/(mcC - mcA)$$

or

$$cf = (hB - hA)/(hC - hA)$$

Output		
moisture content of inlet air	0.0068	
moisture content at ADP	0.0106	
moisture content of outlet air	0.0095	
make-up water req.	0.0054	kg/s
Spec. enthalpy at inlet	41.4	kJ/kg
Spec. enthalpy at ADP	42.0	kJ/kg
Spec. enthalpy at outlet	41.8	kJ/kg
Dry-bulb temp at outlet	17.70	C

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## Appendix B

Determine the adiabatic saturation temperature of air at the

following conditions:

dry-bulb temperature                    22 degC

wet-bulb temperature (sling)        14 degC

An adiabatic process is defined as a process in which no external heat enters or leaves the system under consideration.

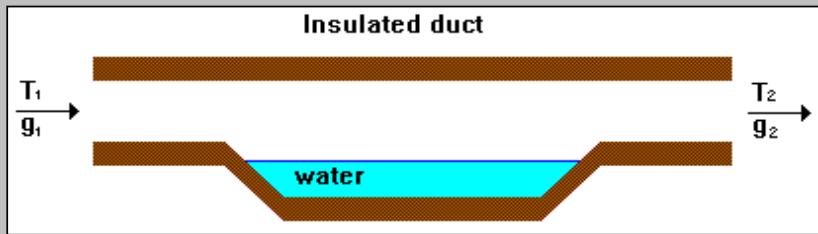
**Adiabatic humidification process:** Air is flowing through a perfectly insulated duct with an open water tank in the bottom of it. If the tank is infinitely long, the air at the outlet will be 100% saturated.

**Inlet:** dry-bulb temperature  $T_1$  and moisture content  $g_1$

**Outlet:** dry-bulb temperature  $T_2$  and moisture content  $g_2$

We may write:  $h_1 = h_2$  or **Sensible heat loss = Latent heat gain** i.e.

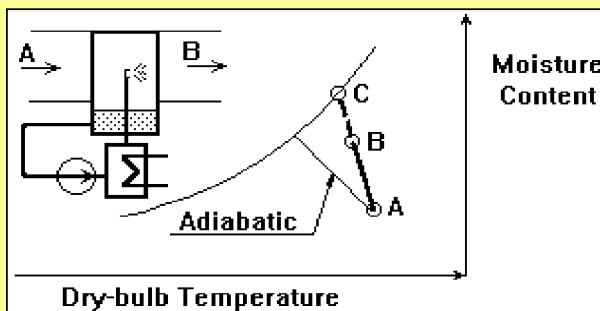
$$C_p * (T_1 - T_2) = H_f g * (g_2 - g_1)$$



Inputs		Units	Error ?
Dry-bulb temperature = $T_1 = T_d$	22.0	C	
Wet-bulb temperatrure	14.0	C	
Atmospheric pressure	1.013	C	
Outputs			
Moisture content = $g_1 = \text{InletMC}$	0.0066	kg/kg	
Spec. heat capacity at inlet = $C_p$	1.0102	kJ/(kg.K)	
Spec. enthalpy at inlet = $\text{InletH}$	38.7	kJ/kg	
Assume that adiabatic saturation temperature $T_{sat}$ , is 30 degC	13.8	C	Assumed
Saturated air has the same temp.			
for dry and wet bulb which results			
into the following			
moisture content at outlet=OutletMC	0.0098	kg/kg	
Now the enthalpy at outlet can be			
calculated. OutletH is:	38.7	kJ/kg	
We know that in an adiabatic			
process diff = $\text{OutletH} - \text{InletH} = 0$	0.0001		Goal
Now, use the solver to adjust cell			
$T_{sat}$ , until the goal cell			
diff is zero.			
Adiabatic Saturation Temp. = $T_{sat}$ =	13.8	C	
<b>Taftan Data</b>			
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## Appendix C

In an air conditioning plant, air flow rate of 2 kg/s passes through a spray water humidifier with a contact factor 0.7. The calorifier provides 40 kW. Determine the moisture content and temperature of the air leaving the humidifier and the amount of make-up water needed. The dry and wet-bulb temperature of the inlet air are 9 °C and 3 °C respectively.



Inputs		Units
Inlet air, DBT	9.00	°C
Inlet air, WBT	3.00	°C
Inlet air, mass flow rate	2.00	kg/s
Contact factor of the humidifier	0.70	
Heat provided by the calorifier	40.00	kW
Atmospheric pressure	1.01	bar

The contact factor of a humidifier is defined as the efficiency for humidification. A 100% efficient humidifier will bring the moisture content of the air to the saturation moisture content at the apparatus dew-point, mcC. The contact factor of the humidifier can be defined by the moisture content differences:

$$cf = (mcB - mcA)/(mcC - mcA)$$

or

$$cf = (hB - hA)/(hC - hA)$$

Output		
moisture content of inlet air	0.0022	
Spec. enthalpy at inlet	14.50	kJ/kg
Spec. enthalpy at outlet	34.50	kJ/kg
Spec. enthalpy at ADP	43.07	kJ/kg
Temperature at ADP	15.38	°C
moisture content at ADP	0.0109	
Estimate spec. enthalpy at ADP	43.07	kJ/kg
Diff = Estimated(h) - h = 0	0.0001	
Use solver to reach the goal		Goal
moisture content of outlet air	0.0083	
make-up water req.	0.0122	kg/s
Dry-bulb temp at outlet	13.50	°C

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## Appendix D

Determine the vapor pressure, moisture content, percentage saturation, relative humidity, specific enthalpy, specific heat capacity, specific entropy and density for air with the following conditions:

dry-bulb temperature      22 degC  
wet-bulb temperature (sling)      14 degC

Inputs		Units	Error ?
Dry-bulb temperature	22.0	C	
Wet-bulb temperatrure	14.0	C	
Atmospheric pressure	1.013	bar	
Outputs			
Moisture content	0.0066		
Percentage saturation	0.3982		
Relative humidity	0.4003		
Gas Constant	0.2882	kJ/(kg.K)	
Specific heat capacity	1.0102	kJ/(kg.K)	
Specific enthalpy	38.7042	kJ/kg	
Specific entropy	0.0782	kJ/(kg.K)	
Density	0.0168	kg/m3	
Molecular mass	28.8525	kg/kmol	
Vapor pressure=Patm*mc/(mc+0.622)	0.0106	bar	

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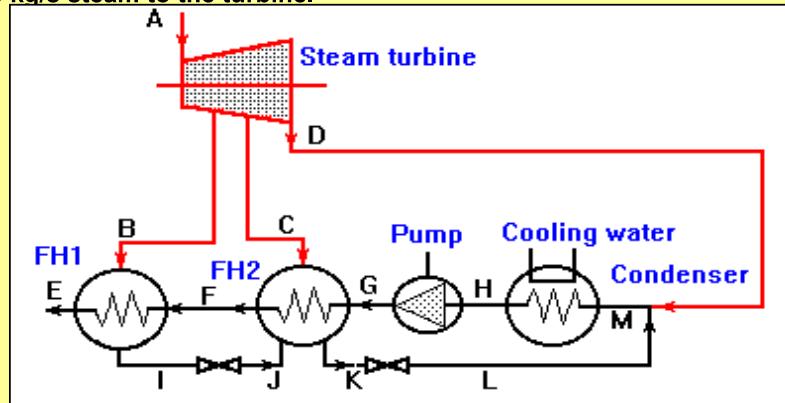
## Closed feed heater

## Appendix E

A regenerative steam cycle uses two closed-feed heaters. Determine the amount of steam bled at each stage. It is known that:

$pB=10 \text{ bar}$ ,  $hB=3033 \text{ kJ/kg}$ ,  $pC=1.0 \text{ bar}$ ,  $hC=2590 \text{ kJ/kg}$ ,  $pG=40 \text{ bar}$ ,  $hG=112 \text{ kJ/kg}$

**Boiler supplies 10 kg/s steam to the turbine.**



Inputs		Units	Error ?
Spec. enthalpy at B	3033.00	kJ/kg	
Spec. enthalpy at C	2590.00	kJ/kg	
Spec. enthalpy at G	112.00	kJ/kg	
Pressure at B	10.00	bar	
Pressure at C	1.00	bar	
Pressure at G	40.00	bar	
Mass flow through the system	10.00	kg/s	
Outputs			
For the throttling process, I-J			
$h_E = h_I = h_J$	762.61	kJ/kg	
For the throttling process, K-L			
$h_F = h_K = h_L$	417.51	kJ/kg	
Energy balance on FH1 gives, mB	1.52	kg/s	
Energy balance on FH2 gives, mC	1.16	kg/s	

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## Appendix F

Dry anthracite with the following composition by mass:

C 90%; H 3%; O 2%; N 1%; S 1%; ash 3%

has been burned in a boiler, when 150% excess air is supplied.

Combustion efficiency is 0.75 Calculate:

1- the stoichiometric air-to-fuel (A/F) ratio

2- the A/F ratio

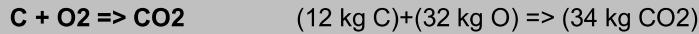
3- analysis of combustion products (dry and wet)

4- temperature of exhaust gases

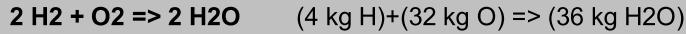
Air is supplied at atmospheric pressure and 18 C with 0.008 specific humidity. The fuel has an average temperature of 35 C when enters the boiler. The net calorific value of the fuel at 15 C is 33 500 kJ/kg  
The specific heat capacity of fuel is 3.2 kJ/kg,K.

### Combustion Equations

Combustion equation for coal:



Combustion equation for hydrogen:



Combustion equation for sulphur:



<b>Fuel Analysis</b>			
<b>Constituent</b>	<b>Mass fraction</b>	<b>Required oxygen kg/kg fuel</b>	<b>Product mass kg/kg fuel</b>
Carbon	0.900	2.400	3.300
Hydrogen	0.030	0.240	0.270
Oxygen	0.020	-0.020	0.000
Nitrogen	0.010	0.000	0.010
Sulphur	0.010	0.010	0.020
Ash	0.030	0.000	0.030
	<b>1.000</b>	2.630	3.630
<b>Analysis of Supplied Air</b>			
Specific Humidity	0.008		
<b>Composition by mass</b>			
<b>Constituent</b>	<b>Dry Air</b>	<b>Humid Air</b>	
N <sub>2</sub>	0.76280	0.75670	
O <sub>2</sub>	0.23290	0.23104	
CO <sub>2</sub>	0.00300	0.00298	
Ar	0.00130	0.00129	
H <sub>2</sub> O	0.00000	0.00800	
SO <sub>2</sub>	0.00000	0.00000	
	<b>1.00000</b>	<b>1.00000</b>	

Combustion of coal

Air required per kg of fuel	11.38	Stoichiometric A/F ratio	kg/kg
Excess Air	1.5		
Actual A/F ratio kg/kg	28.45867		
<b>Exhaust Gases</b>		<b>Wet Mass</b>	<b>Dry Mass</b>
<b>Constituent</b>	<b>Mass</b>	<b>Composition</b>	<b>Composition</b>
N2	21.54461	0.73210	0.74469
O2	3.94500	0.13405	0.13636
CO2	3.38469	0.11501	0.11699
Ar	0.03670	0.00125	0.00127
H2O	0.49767	0.01691	0.00000
SO2	0.02000	0.00068	0.00069
	<b>29.42867</b>	<b>1.00000</b>	<b>1.00000</b>
<b>Exhaust Gases</b>			<b>Volume</b>
<b>Constituent</b>	<b>Kg/kmol</b>	<b>Mole Fraction</b>	<b>Composition</b>
N2	28	0.02615	0.77058
O2	32	0.00419	0.12346
CO2	44	0.00261	0.07704
Ar	40	0.00003	0.00092
H2O	18	0.00094	0.02769
SO2	64	0.00001	0.00031
		0.03393	1.00000
<b>Mass balance</b>			
<b>Fuel</b>	1.00000		
<b>Supplied Air</b>	28.45867		
	<b>29.45867</b>		
<b>Exhaust Gases</b>	29.42867		
<b>Ash</b>	0.03000		
	<b>29.45867</b>		
Supplied Air Temp.	18	C	
Fuel Cp	3.2	kJ/(kg.K)	
Net Calorific Value	33500	kJ/kg	
Combustion efficiency	0.75		
	<b>Enthalpy</b>	<b>Mass Flow</b>	<b>m*h</b>
	<b>kJ/kg</b>	<b>kg/s</b>	<b>kJ/s</b>
<b>Supplied Air</b>	38.31	28.46	1090.14
<b>Fuel</b>	64.00	1.00	64.00
<b>Fuel Energy Supplied</b>	33500.00	1.00	25125.00
			<b>26279.14</b>
<b>Exhaust Gases</b>	892.07		
<b>Exhaust Gases Temp</b>	774.	C	
<b>Taftan Data</b>			
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## Appendix G

A biomass fuel with the following composition by mass:

C 54%; H 22%; O 12%; N 4%; S 1.3%; ash 6.7%

C<sub>1</sub>, percentage carbon on the dry ash-free basis 17%  
has been burned in a boiler, when 150% excess air is supplied.  
Combustion efficiency is 0.75 Calculate:

1- the stoichiometric air-to-fuel (A/F) ratio

2- the A/F ratio

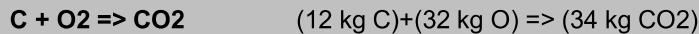
3- analysis of combustion products (dry and wet)

4- temperature of exhaust gases

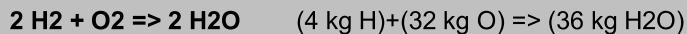
Air is supplied at atmospheric pressure and 18 C with 0.008 specific humidity. The fuel has an average temperature of 35 C when enters the boiler. Use Vondracek formula to estimate the net calorific value of the fuel. The specific heat capacity of fuel is 3.2 kJ/kg,K.

### Combustion Equations

Combustion equation for coal:



Combustion equation for hydrogen:



Combustion equation for sulphur:



<b>Fuel Analysis</b>			
<b>Constituent</b>	<b>Mass fraction</b>	<b>Required oxygen kg/kg fuel</b>	<b>Product mass kg/kg fuel</b>
Carbon	0.540	1.440	1.980
Hydrogen	0.220	1.760	1.980
Oxygen	0.120	-0.020	0.100
Nitrogen	0.040	0.000	0.040
Sulphur	0.013	0.013	0.026
Ash	0.067	0.000	0.067
	<b>1.000</b>	3.193	4.193
Carbon on dry ash-free basis	0.170		
<b>Analysis of Supplied Air</b>			
Specific Humidity	0.008		
<b>Composition by mass</b>			
<b>Constituent</b>	<b>Dry Air</b>	<b>Humid Air</b>	
N <sub>2</sub>	0.76280	0.75670	
O <sub>2</sub>	0.23290	0.23104	
CO <sub>2</sub>	0.00300	0.00298	
Ar	0.00130	0.00129	
H <sub>2</sub> O	0.00000	0.00800	
SO <sub>2</sub>	0.00000	0.00000	

Combustion of biomass fuel

	<b>1.00000</b>	<b>1.00000</b>	
Air required per kg of fuel	13.82	Stoichiometric A/F ratio	kg/kg
Excess Air	1.5		
Actual A/F ratio kg/kg	34.55077		
<b>Exhaust Gases</b>		<b>Wet Mass</b>	<b>Dry Mass</b>
<b>Constituent</b>	<b>Mass</b>	<b>Composition</b>	<b>Composition</b>
N2	26.18449	0.74001	0.79042
O2	4.78950	0.13536	0.14458
CO2	2.08282	0.05886	0.06287
Ar	0.04456	0.00126	0.00135
H2O	2.25641	0.06377	0.00000
SO2	0.02600	0.00073	0.00078
	<b>35.38377</b>	<b>1.00000</b>	<b>1.00000</b>
<b>Exhaust Gases</b>			<b>Volume</b>
<b>Constituent</b>	<b>Kg/kmol</b>	<b>Mole Fraction</b>	<b>Composition</b>
N2	28	0.02643	0.74275
O2	32	0.00423	0.11888
CO2	44	0.00134	0.03760
Ar	40	0.00003	0.00088
H2O	18	0.00354	0.09956
SO2	64	0.00001	0.00032
		0.03558	1.00000
<b>Mass balance</b>			
<b>Fuel</b>	<b>1.00000</b>		
<b>Supplied Air</b>	<b>34.55077</b>		
	<b>35.55077</b>		
<b>Exhaust Gases</b>	35.38377		
<b>Ash</b>	0.06700		
	<b>35.45077</b>		

Vondracek suggests the following formula for gross calorific value (GCV) of fossil fuels when oxygen content exceeds 10%

$$\text{GCV} = (337 - 0.261 C_1) C + 1130 (H - O/10) + 105 S$$

GCV is in (kJ/kg). C, H, O, S are percentages on weight basis for carbon, hydrogen, oxygen and sulphur. The net calorific value for a constant pressure combustion is:

$$\text{NCV} = \text{GCV} - mc * h_{fg}$$

mc is the mass of condensate per unit quantity of fuel and h<sub>fg</sub> is the latent heat of steam at 25 degree Celsius which is 2442 kJ/kg.

Supplied Air Temp.	18		
Fuel Cp	3.2	<b>kJ/(kg.K)</b>	
Gross Calorific Value, GCV	41836	<b>kJ/kg</b>	
Net Calorific Value, NCV	41680	<b>kJ/kg</b>	
Combustion efficiency	0.75		
	<b>Enthalpy</b>	<b>Mass Flow</b>	<b>m*h</b>

Combustion of biomass fuel

	<b>kJ/kg</b>	<b>kg/s</b>	<b>kJ/s</b>
<b>Supplied Air</b>	38.31	34.55	1323.51
<b>Fuel</b>	64.00	1.00	64.00
<b>Fuel Energy Supplied</b>	41680.38	1.00	31260.28
			<b>32647.79</b>
<b>Exhaust Gases</b>	918.34	35.55	32647.79
<b>Exhaust Gases Temp</b>	671.	C	

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## Appendix H

A fossil fuel with the following composition by mass:

C 70%; H 18.5%; O 3%; N 4%; S 1.5%; ash 3%

has been burned in a boiler, when 100% excess air is supplied.

Combustion efficiency is 0.75 Calculate:

1- the stoichiometric air-to-fuel (A/F) ratio

2- the A/F ratio

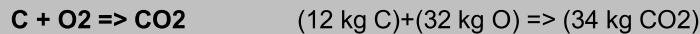
3- analysis of combustion products (dry and wet)

4- temperature of exhaust gases

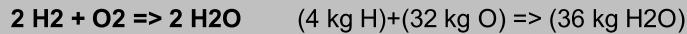
Air is supplied at atmospheric pressure and 18 C with 0.008 specific humidity. The fuel has an average temperature of 35 C when enters the boiler. Use Dulong formula to estimate the net calorific value of the fuel. The specific heat capacity of fuel is 3.2 kJ/kg,K.

### Combustion Equations

Combustion equation for coal:



Combustion equation for hydrogen:



Combustion equation for sulphur:



<b>Fuel Analysis</b>			
<b>Constituent</b>	<b>Mass fraction</b>	<b>Required oxygen kg/kg fuel</b>	<b>Product mass kg/kg fuel</b>
Carbon	0.700	1.867	2.567
Hydrogen	0.185	1.480	1.665
Oxygen	0.030	-0.020	0.010
Nitrogen	0.040	0.000	0.040
Sulphur	0.015	0.015	0.030
Ash	0.030	0.000	0.030
	<b>1.000</b>	3.342	4.342
<b>Analysis of Supplied Air</b>			
Specific Humidity	0.008		
<b>Composition by mass</b>			
<b>Constituent</b>	<b>Dry Air</b>	<b>Humid Air</b>	
N <sub>2</sub>	0.76280	0.75670	
O <sub>2</sub>	0.23290	0.23104	
CO <sub>2</sub>	0.00300	0.00298	
Ar	0.00130	0.00129	
H <sub>2</sub> O	0.00000	0.00800	
SO <sub>2</sub>	0.00000	0.00000	
	<b>1.00000</b>	<b>1.00000</b>	

Air required per kg of fuel	14.46	Stoichiometric A/F ratio	kg/kg
Excess Air	1		
Actual A/F ratio kg/kg	28.92757		
<b>Exhaust Gases</b>		<b>Wet Mass</b>	<b>Dry Mass</b>
<b>Constituent</b>	<b>Mass</b>	<b>Composition</b>	<b>Composition</b>
N2	21.92942	0.73373	0.78344
O2	3.34167	0.11181	0.11938
CO2	2.65276	0.08876	0.09477
Ar	0.03730	0.00125	0.00133
H2O	1.89642	0.06345	0.00000
SO2	0.03000	0.00100	0.00107
	<b>29.88757</b>	<b>1.00000</b>	<b>1.00000</b>
<b>Exhaust Gases</b>			<b>Volume</b>
<b>Constituent</b>	<b>Kg/kmol</b>	<b>Mole Fraction</b>	<b>Composition</b>
N2	28	0.02620	0.74260
O2	32	0.00349	0.09901
CO2	44	0.00202	0.05716
Ar	40	0.00003	0.00088
H2O	18	0.00353	0.09990
SO2	64	0.00002	0.00044
		0.03529	1.00000
<b>Mass balance</b>			
<b>Fuel</b>	1.00000		
<b>Supplied Air</b>	28.92757		
	<b>29.92757</b>		
<b>Exhaust Gases</b>	29.88757		
<b>Ash</b>	0.03000		
	<b>29.91757</b>		

Dulong suggests the following formula for gross calorific value (GCV) of fossil fuels when oxygen content is less than 10%

$$\text{GCV} = 337 \text{ C} + 1442 (\text{H} - \text{O}/8) + 93 \text{ S}$$

GCV is in (kJ/kg). C, H, O, S are percentages on weight basis for carbon, hydrogen, oxygen and sulphur. The net calorific value for a constant pressure combustion is:

$$\text{NCV} = \text{GCV} - mc * hfg$$

mc is the mass of condensate per unit quantity of fuel and hfg is the latent heat of steam at 25 degree Celsius which is 2442 kJ/kg.

Supplied Air Temp.	18		
Fuel Cp	3.2	<b>kJ/(kg.K)</b>	
Gross Calorific Value, GCV	49866	<b>kJ/kg</b>	
Net Calorific Value, NCV	49711	<b>kJ/kg</b>	
Combustion efficiency	0.75		
	<b>Enthalpy</b>	<b>Mass Flow</b>	<b>m*h</b>
	<b>kJ/kg</b>	<b>kg/s</b>	<b>kJ/s</b>

Combustion of Fossil Fuels.xls

<b>Supplied Air</b>	38.31	28.93	1108.10
<b>Fuel</b>	64.00	1.00	64.00
<b>Fuel Energy Supplied</b>	49710.80	1.00	37283.10
			<b>38455.21</b>
<b>Exhaust Gases</b>	1284.94	29.93	38455.21
<b>Exhaust Gases Temp</b>	964.	C	

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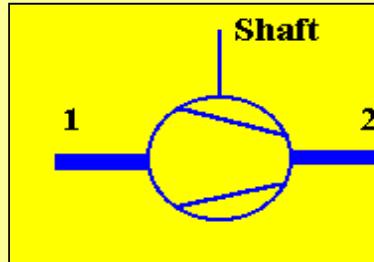
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# Appendix I

Air at 1.013 bar and 25 C with 0.005 specific humidity enters to a compressor with a pressure ratio of 10/1. The isentropic efficiency of the compressor is 0.82.

Calculate the temperature, specific enthalpy, and specific entropy of air at the outlet.

If the air intake is 5 kg/s, what is the compressor work on the fluid?



Inputs		Units	Error ?
Inlet Pressure	1.013	bar	
Inlet Temperature	25.000	C	
Specific Humidity (moisture content)	0.005		
Isentropic Efficiency	0.820		
Pressure Ratio	10.000		
Mass Flow	5.000	kg/s	

## Equations:

$$\gamma = \frac{C_p}{C_p - R}$$

$$\eta_c = \frac{H_{2s} - H_1}{H_2 - H_1} \quad \text{Isentropic Efficiency}$$

$$\frac{T_{2s}}{T_1} = \left( \frac{P_2}{P_1} \right)^{\frac{\gamma-1}{\gamma}} \quad \text{Isentropic Process}$$

Outputs			
Inlet Enthalpy	37.759	kJ/kg	
Inlet Entropy	0.088	kJ/(kg.K)	
Inlet Specific Heat Capacity	1.009	kJ/(kg.K)	
Gas Constant	0.288	kJ/(kg.K)	
Gamma	1.399		
Kelvin	273.150	C	
Outlet Pressure	10.130	bar	
Ln(P2/P1)	2.303		
(1-1/Gamma)*Ln(P2/P1)	0.657		
T2s/T1=....	1.929		
T2s	575.142	degree K	
T2s	301.992	C	
H2s	321.712	kJ/kg	
Outlet Enthalpy	384.043	kJ/kg	
Outlet Temperature	360.970	C	

Compression Process

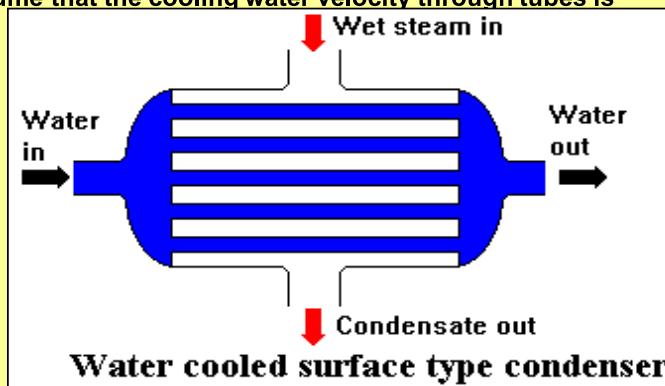
<b>Outlet Entropy</b>	<b>0.197</b>	<b>kJ/kg</b>	
<b>Compressor Work on Fluid</b>	<b>1731.421</b>	<b>kW</b>	
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## Appendix J

A surface condenser is required to deal with 15 000 kg/h wet steam. Wet steam temperature is 37 C and enters the condenser with 0.95 quality (dryness fraction is 0.95). The water used for cooling has the following data:

- inlet pressure 1.20 bar, inlet temperature 7 C
- outlet pressure 1.013 bar, outlet temperature 22 C

Calculate the flow rate of cooling water and tube surface of the condenser. Assume that the cooling water velocity through tubes is 1.5 m/s



Inputs		Units	Error ?
Wet steam inlet temperature	37	C	
Steam quality	0.95		
Cooling water inlet temperature	7	C	
Cooling water inlet pressure	1.2	bar	
Cooling water outlet temperature	22	C	
Cooling water outlet pressure	1.013	bar	
Steam mass flow	15000	kg/h	
Cooling water speed	1.5	m/s	
Outputs			
Wet steam pressure	0.06274	bar	
Enthalpy of steam at inlet	2448.28	kJ/kg	
Enthropy of condensate	154.92	kJ/kg	
Rejected heat/hour	34400440.44	kJ/h	
Rejected heat/second	9555.68	kW	
Enthalpy of water at inlet	29.53	kJ/kg	
Enthalpy of water at outlet	92.32	kJ/kg	
Water mass flow	547848.07	kg/h	

The overall heat transfer coefficient can be calculated according to BEAMA or HEI standards.

BEAMA : British Electrical and Allied Manufacturers Association

BEAMA publication on the recommended practice for design of surface type steam condenser

HEI : Heat Exchanger Institute

HEI standards for steam surface condensers

**According to BEAMA:**

$$U = 2.15 v^{0.5} (0.7586 + 0.0135 T - 0.0001 T^2)$$

**According to HEA:**

$$U = 2.70 v^{0.5} (0.5707 + 0.0274 T - 0.00036 T^2)$$

**v : Water speed in tubes**

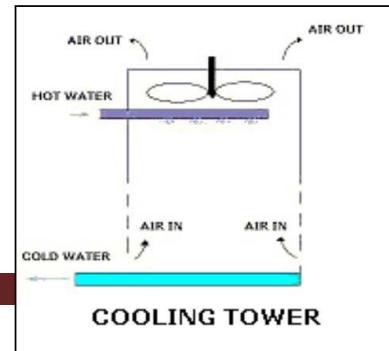
<b>T : Condenser temperature [C]</b>			
<b>U : Overall heat transfer coefficient [kW/m<sup>2</sup> K]</b>			
Outputs		Unit	
Heat transfer coeff.(BEAMA)	2.95235	kW/m <sup>2</sup> ,K	
Logarithmic mean temp. diff.	49.83	degree K	
Required area	64.96	m <sup>2</sup>	
If we use the less conservative HEI method we obtain the following:			
Outputs		Unit	
Heat transfer coeff.(HEI)	3.60991	kW/m <sup>2</sup> ,K	
Required area	53.12	m <sup>2</sup>	
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## Appendix K

**COOLING TOWER**

Water inlet mass flow rate	5.5 kg/s
Water inlet temperature	44 C
Induced air flow rate	9 m3/s
Power absorbed by air (power used by fan)	4.75 kW
Inlet air temperature	18 C
Inlet air relative humidity	60 %
Outlet air temperature	26 C
Outlet air relative humidity	100 %
Air pressure thru tower	1.013 bar

Calculate  
mass flow rate of make-up water  
Final temperature of water leaving the cooling tower



At inlet

Pg	0.021 bar
partial pressure of water	0.012 bar
Partial pressure of other gases in inlet air	1.001 bar
Mass flow rate of air (dry)	10.783 kg/s
Mass flow rate of water in the air	0.083 kg/s
moisture content	0.008

At Exit

Pg	0.034 bar
specific humidity/moisture content	0.021
Mass flow rate of water in the air	0.230 kg/s
Make-up water req.	0.147 kg/s
Water leaving the cooling tower	5.353 kg/s

Applying steady-flow condition	m[kg/s]	h[kJ/kg]	m*h[kJ/s]
Inlet air	10.866	37.51	407.55
Outlet air	11.013	80.66	888.28
Inlet water	5.500	184.25	1013.38
Outlet water	5.353	100.40	537.40

Outlet water temperature	23.9 C
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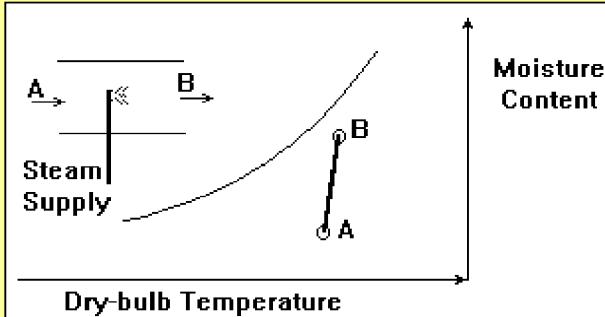
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## Appendix L

In an air conditioning plant, air flow rate of 2 kg/s passes through a steam humidifier. Determine the load on the humidifier and the steam supplied. The dry and wet-bulb temperature of the inlet air are 9 C and 3 C respectively. Air leaves the humidifier with a moisture content of 0.008



Inputs		Units
Inlet air, DBT	9.00	C
Inlet air, WBT	3.00	C
Inlet air, mass flow rate	2.00	kg/s
Outlet air, moisture content	0.008	
Atmospheric pressure	1.01	bar

Steam can be directly injected to air stream for air conditioning purposes. In this process, all the latent heat necessary for evaporation of water is added outside the air stream. The supply of water vapor increases the enthalpy of the air. The temperature increase in this process is negligible and it can be assumed as an isothermal process with good approximation. Load on humidifier is:

$$Q = m_A * (h_B - h_A)$$

and the steam supplied by humidifier is:

$$m_{\text{Steam}} = m_A * (m_c B - m_c A)$$

Output		
moisture content of inlet air	0.0022	
Outlet air, DBT	9.0000	
Spec. enthalpy at inlet	14.5	kJ/kg
Spec. enthalpy at outlet	29.2	kJ/kg
Load on the humidifier	29.4102	kW
steam supplied	0.0117	kg/s

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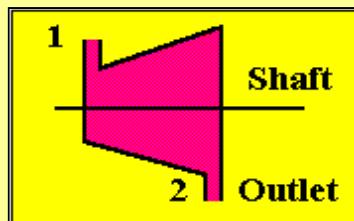
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## Appendix M

Flue gases at 10.5 bar and 700 C enter to a gas turbine. The turbine has a pressure ratio of 10/1. The isentropic efficiency of the expansion is 0.85. The volumetric composition of flue gases is:

N<sub>2</sub> 76.4%; O<sub>2</sub> 4.0%; CO<sub>2</sub> 15.1%; Ar 0.09%; H<sub>2</sub>O 4.2%; SO<sub>2</sub> 0.21%

Calculate the temperature, specific enthalpy, and specific entropy of the flue gases at the outlet. If the intake of hot gases is 5 kg/s, what is the output of the turbine?



Inputs		Units	Error ?
Inlet Pressure	10.5	bar	
Inlet Temperature	700.0	C	
N <sub>2</sub> Volumetric %	0.7640		
O <sub>2</sub> Volumetric %	0.0400		
CO <sub>2</sub> Volumetric %	0.1510		
Ar Volumetric %	0.0009		
H <sub>2</sub> O Volumetric %	0.0420		
SO <sub>2</sub> Volumetric %	0.0021		
Isentropic Efficiency	0.850		
Pressure Ratio	10.000		
Mass Flow	5.000	kg/s	

Equations:

$$\gamma = \frac{C_p}{C_p - R}$$

$$\eta_t = \frac{H_1 - H_2}{H_1 - H_{2s}} \quad \text{Isentropic Efficiency}$$

$$\frac{T_1}{T_{2s}} = \left( \frac{P_1}{P_2} \right)^{\frac{\gamma-1}{\gamma}} \quad \text{Isentropic Process}$$

Outputs			
Inlet Enthalpy	833.088	kJ/kg	
Gas Constant	0.275	kJ/(kg.K)	
Inlet Entropy	0.726	kJ/(kg.K)	
Inlet Specific Heat Capacity	1.198	kJ/(kg.K)	
Gamma	1.298		
Kelvin	273.150	C	
Outlet Pressure	1.050	bar	
Ln(P1/P2)	2.303		

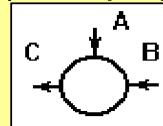
(1-1/Gamma)*Ln(P1/P2)	0.528			
T1/T2s=....	1.696			
T2s	573.923	C		
T2s	300.773	C		
H2s	376.256	kJ/kg		
Outlet Enthalpy	444.781	kJ/kg		
Outlet Temperature	363.341	C		
Outlet Entropy	0.871	kJ/(kg.K)		
Turbine Output	1941.536	kW		
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## Appendix N

In a Rankine cycle, wet steam (3.5 bar with  $q = 0.83$ ) is bled off for heating purpose. The bleed steam and feed water (3.5 bar and 135 C) from a pump are mixed in the feed heater.

Determine the quantity of bleed steam.

The steam supplied from the boiler is 5 kg/s



Inputs		Units	Error ?
Pressure at A, B and C	3.5	bar	
Steam quality at A	0.83		
Steam Temp. at B	135	C	
Steam quality at C	0		
Mass Flow	5.00	kg/s	
Outputs			
Spec. enthalpy at A	2366.57	kJ/kg	
Spec. enthalpy at B	567.7011	kJ/kg	
Spec. enthalpy at C	584.27	kJ/kg	
Energy and mass balance			
Eq1: $m_A + m_B - m_C = 0$			
Eq2: $m_A \cdot h_A + m_B \cdot h_B - m_C \cdot h_C = 0$			
mass flow of bleed steam	0.046	kg/s	

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## Appendix O1

Estimate the specific volume of dichlorodifluoromethane vapor  
at 20,67 bar and 366,5 K

Tc	385 K	Critical temperature	Table look up from file: "Chemical component properties.xls"
Pc	41.2 bar	Critical pressure	"Chemical component properties.xls"
Omega	0.176	Acentric factor	Index 212

P 20,67 bar

T 366,5 K

R 83.14 cm<sup>3</sup>.bar/(mol.K)

**Solution:**

Tr 0.952

Pr 0.502

Z 0.745

V=ZRT/P 1098 cm<sup>3</sup>/mol

Lee-Kesler method

V experimental 1109 cm<sup>3</sup>/mol

Registered Version.

Error -1.0%

Temperature range for Lee-Kesler method

Pressure range for Lee-Kesler method

Tmin 115.5 K

Pmin 0.412 bar

Tmax 1540 K

Pmax 412 bar

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## Appendix O2

Estimate the specific volume of the saturated isobutane at 300 K

Tc	408.1 K
Pc	36.5 bar
Omega	0.283
R	83.14 cm <sup>3</sup> .bar/(mol.K)

T 300 K

**Solution:**

Tr	0.735
Pr	0.084
Z	0.012
Ps	3.078
Ps experimental	3.704

Zc	0.265
Zc Experimental	0.283
Error	-6.3%

V=ZRT/P	97.88 cm <sup>3</sup> /mol
VL experimental	105.90 cm <sup>3</sup> /mol
Error	-7.6%

Vc	246.545 cm <sup>3</sup> /mol
Vc Experimental	263.000 cm <sup>3</sup> /mol
Error	-6.3%

Vv	6091.78 cm <sup>3</sup> /mol
Vv experimental	6031.00 cm <sup>3</sup> /mol
Error	1.0%

Temperature range for Lee-Kesler method	
Tmin	122.43 K
Tmax	1632.4 K

Pressure range for Lee-Kesler method	
Pmin	0.365 bar
Pmax	365 bar

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## Appendix O3

Specific Volume of CHLOROBENZENE at its normal boiling point

**Solution:**

Fluid name	CHLOROBENZENE		
Fluid index	182		
Tc	359.25 C	Critical temperature (table look up)	
Tc in Kelvin	632.4 K		
Pc	45.2 bar	Critical pressure (table look up)	
P	1.013 bar		
Pr	0.022412		
Acentric Factor	0.249	Acentric factor (table look up)	
Tr	0.640942		
Tb	405.332 K		
Tb(experimental)	131.75 C	404.9 K	Error
R	83.14 cm <sup>3</sup> .bar/(mol.K)		
Z(Liquid)	0.003554		

$$V = Z \cdot R \cdot T / P = Z \cdot G_c \cdot T / P$$

V(Liquid)	118.11 cm <sup>3</sup> /mol
V(Liquid) experimental	115.00 cm <sup>3</sup> /mol
Error	2.7%

Temperature range for Lee-Kesler method	Pressure range for Lee-Kesler method
Tmin	Pmin 0.452 bar
Tmax	Pmax 452 bar

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## Appendix O4

Estimate the specific volume of isobutane  
 case 1- saturated liquid at 310.93 K  
 case 2- compressed liquid at 310.93 K and 137.9 bar

**Solution:**

Fluid name	isobutane
Fluid index	274
Tc in Kelvin	408.1 K
Pc	36.5 bar
T	310.93 K
P	137.9 bar
Pr	3.78
Acentric Factor	0.176
Tr	0.76
R	83.14 cm <sup>3</sup> .bar/(mol.K)

Table look up from file:  
 "Chemical component properties.xls"  
 Index 274

P <sub>sat</sub> (reduced)	0.139353
P <sub>sat</sub>	5.086 bar
P <sub>sat</sub> experimental	4.958 bar
Error	2.6%

Z(T <sub>sat</sub> )	0.021138
V(T <sub>sat</sub> )	107.4 cm <sup>3</sup> /mol
V(T <sub>sat</sub> ) experimental	108.2 cm <sup>3</sup> /mol
Error	-0.7%

Z(P,T)	0.556481
V(P,T)	104.3 cm <sup>3</sup> /mol
V(P,T) experimental	102.7 cm <sup>3</sup> /mol
Error	1.6%

Temperature range for Lee-Kesler method	Pressure range for Lee-Kesler method
Tmin	Pmin 0.365 bar
Tmax	Pmax 365 bar

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## Appendix O5

Estimate the enthalpy and entropy departures for Propylene at 398.15 K and 100 bar.

The ideal gas reference pressure for entropy is 1 bar.

**Solution:**

Fluid Name	Propylene	
Fluid index	416	
Molecular mass	42.081	
Pc	46.2 bar	
Tc	91.85 C	365 K
Acentric fac.	0.148	
P	100 bar	
T	398.15 K	
R	8.314 kJ/(kg.K)	
Pr	2.16	
Tr	1.09	
P0	1.00 bar	

H0-H	240.80 kJ/kg
(H0-H) experimental	244.58 kJ/kg
Error	-1.5%

S0-S	1.3838 kJ/(kg.K)
(S0-S) experimental	1.4172 kJ/(kg.K)
Error	-2.4%

Temperature range for Lee-Kesler method	Pressure range for Lee-Kesler method		
Tmin	Pmin	0.462 bar	
Tmax	Pmax	462 bar	

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## Appendix P

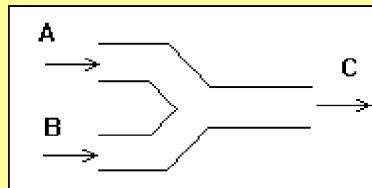
In an air conditioning plant, outdoor air mixes with recirculated air. Calculate the specific enthalpy, moisture content and dry-bulb temperature of the mixed air stream.

Outdoor air:

dry-bulb temp. = 5 C  
moisture content = 0.002  
mass flow = 2 kg/s

Recirculated air:

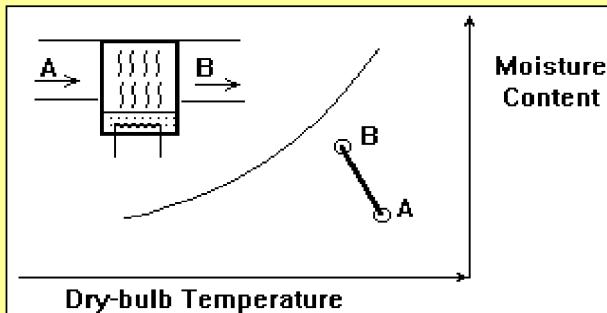
dry-bulb temp. = 21 C  
moisture content = 0.012  
mass flow = 6 kg/s



Inputs		Units
Outdoor air, DBT	5.00	C
Outdoor air, moisture content	0.002	
Outdoor air, mass flow rate	2.00	kg/s
Recirculated air, DBT	21.00	C
Recirculated air, moisture content	0.010	
Recirculated air, mass flow rate	6.00	kg/s
Outputs		
mass flow rate of the mixture	8.00	kg/s
moisture content of the mixture	0.0080	
specific enthalpy of the outdoor air	10.04	kJ/kg
specific enthalpy of the recirculated air	46.43	kJ/kg
specific enthalpy of the mixture	37.33	kJ/kg
Dry-bulb temp. of the mixture	17.04	C
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## Appendix Q

In an air conditioning plant, air flow rate of 2 kg/s passes through a pan steam humidifier. Determine the load on the humidifier and the steam supplied. The dry and wet-bulb temperature of the inlet air are 9 C and 3 C respectively. Air leaves the humidifier with a moisture content of 0.008



Inputs		Units
Inlet air, DBT	9.00	C
Inlet air, WBT	3.00	C
Inlet air, mass flow rate	2.00	kg/s
Outlet air, moisture content	0.008	
Atmospheric pressure	1.01	bar

A pan steam humidifier uses a heating element inside a water tank. The tank is mounted at the bottom of the air duct. The air flowing over the water surface will cause some evaporative cooling which results in drop of air dry-bulb temperature. The ratio of sensible heat to total heat is approximately 0.2. Load on the humidifier is:

$$Q = m_A * (h_B - h_A)$$

and the steam supplied by humidifier is:

$$m_{Steam} = m_A * (m_C B - m_C A)$$

Output			
moisture content of inlet air	0.0022		
Outlet air, DBT	12.66	C	Assumed
Spec. enthalpy at inlet	14.5	kJ/kg	
Spec. enthalpy at outlet	32.9	kJ/kg	
Load on the humidifier = total heat	36.8061	kW	
Sensible heat	7.3591	kJ/kg	
Qs / Q = 0.2	0.1999		Goal
Use the solver to reach the goal			
steam supplied	0.0117	kg/s	

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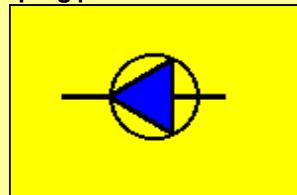
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## Pump

### Appendix R

Saturated water is supplied to a feed-pump at 0.035 bar. The outlet pressure is 12 bar.

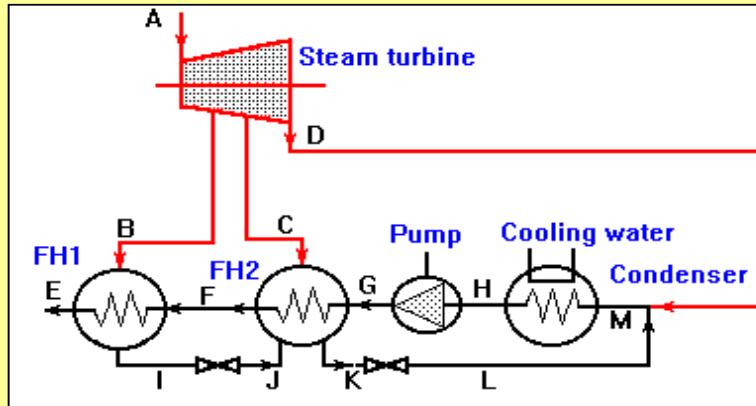
- 1-Calculate the input power to the feed-pump if the mass flow of the water is 2 kg/s and the isentropic efficiency of the pump is 0.9
- 2-Calculate specific enthalpy, specific entropy, specific volume and temperature of the water before and after the pumping process



Inputs		Units	Error ?
Inlet Pressure	0.035	bar	
Saturated Water	0		
Outlet Pressure	12	bar	
Isentropic Efficiency	0.9		
Mass Flow	2	kg/s	
Outputs			
Inlet Enthalpy	111.85	kJ/kg	
Inlet Entropy	0.3907	kJ/(kg.K)	
Inlet Temperature	26.69	C	
Enthalpy of Isentropic Compression	113.20	kJ/kg	
Outlet Enthalpy	113.35	kJ/kg	
Input Power	3.01	kW	
Outlet Temperature	26.79	C	
Outlet Entropy	0.3912	kJ/kg	
Outlet Specific Volume	1.0029	m <sup>3</sup> /ton	
Inlet Specific Volume	1.0033	m <sup>3</sup> /ton	
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## Appendix S

A regenerative steam cycle uses two closed-feed heaters. Determine the amount of steam bled at each stage, the work output of the plant and cycle efficiency. It is known that:  $p_A=40$  bar,  $t_A=500$  C,  $p_B=10$  bar,  $p_C=1.0$  bar,  $p_D=0.035$  bar. Isentropic efficiency of the steam turbine and pump are 0.85 and 0.90 respectively. Boiler supplies 10 kg/s steam to the turbine.



Inputs		Units	Error ?
Pressure at A	40.00	bar	
temperature at A	500.00	C	
Pressure at B	10.00	bar	
Pressure at C	1.00	bar	
Pressure at D	0.035	bar	
Pressure at G	40.00	bar	
Mass flow through the system	10.00	kg/s	
Turbine isentropic eff.	0.85		
Pump isentropic eff.	0.90		
Outputs			
Spec. enthalpy at A	3444.99	kJ/kg	
Spec. entropy at A	7.09	kJ/(kg.K)	
Isentropic enthalpy at B	3032.71	kJ/kg	
Spec. enthalpy at B	3094.55	kJ/kg	
Power generated at stage 1, POW1	3504.33	kW	
Spec. entropy at B	7.20	kJ/(kg.K)	
Isentropic enthalpy at C	2615.07	kJ/kg	
Spec. enthalpy at C	2686.99	kJ/kg	
Power generated at stage 2, POW2	3472.49	kW	
Spec. entropy at C	7.39	kJ/(kg.K)	
Isentropic enthalpy at D	2210.69	kJ/kg	
Spec. enthalpy at D	2282.14	kJ/kg	
Power generated at stage 3, POW3	3003.49	kW	
Spec. enthalpy at H	111.85	kJ/kg	
Spec. entropy at H	0.39	kJ/(kg.K)	
Isentropic enthalpy at G	116.00	kJ/kg	
Spec. enthalpy at G	116.47	kJ/kg	
Power req. for pump	46.21	kW	
For the throttling process, I-J			

### Regenerative steam cycle

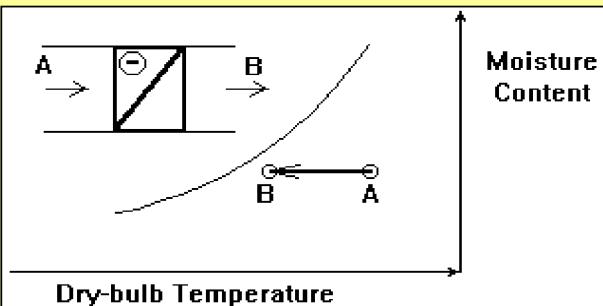
$h_E = h_I = h_J$	762.61	kJ/kg	
For the throttling process, K-L			
$h_F = h_K = h_L$	417.51	kJ/kg	
Energy balance on FH1 gives, mB	1.48	kg/s	
Energy balance on FH2 gives, mC	1.10	kg/s	
Net power generated	9934.10	kW	
Cycle efficiency	0.370		

## Appendix T

In an air conditioning plant, air flow rate of 2 kg/s passes through a coil. The dry-bulb temperature decreases from 25 C to 10 C.

The moisture content of the air is 0.005. Determine the load on the coil. Surface temperature of the coil is above the dew-point temperature i.e.

the moisture content is constant.



Inputs		Units
on-coil air, DBT	25.00	C
on-coil air, moisture content	0.005	
on-coil air, mass flow rate	2.00	kg/s
off-coil air, DBT	10.00	C
off-coil air, moisture content	0.005	
off-coil air, mass flow rate	2.00	kg/s
Atmospheric pressure	1.01	bar

Output		
Dew-point temperature	4.0	C
Specific enthalpy of the on-coil air	37.7592	kJ/kg
Specific enthalpy of the off-coil air	22.6280	kJ/kg
Load on the coil	30.2625	kW

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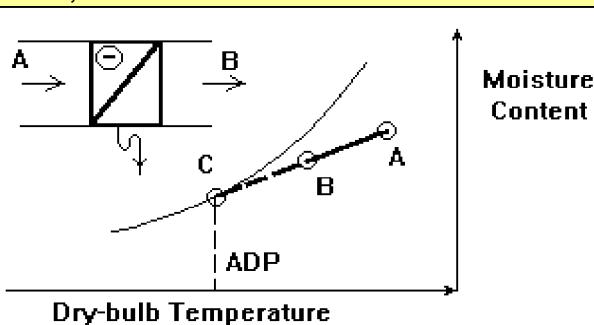
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## Appendix U

In an air conditioning plant, air flow rate of 2 kg/s passes through a coil. The dry-bulb temperature decreases from 24 C to 12 C.

The moisture content of the air decreases from 0.010 to 0.008.

Determine the load on the coil, contact factor of the coil and apparatus dew-point temperature, ADP.



Inputs		Units
on-coil air, DBT	24.00	C
on-coil air, moisture content	0.010	
on-coil air, mass flow rate	2.00	kg/s
off-coil air, DBT	12.00	C
off-coil air, moisture content	0.008	
Atmospheric pressure	1.01	bar

The contact factor of a coil is defined as the efficiency for dehumidification. A 100% efficient coil will bring the moisture content of the air to the saturation moisture content at the apparatus dew-point, mcC. The contact factor of the coil can be defined by moisture content differences:

$$cf = (mcA - mcB)/(mcA - mcC)$$

or

$$cf = (hA - hB)/(hA - hC)$$

Output		
Specific enthalpy of the on-coil air	49.4733	kJ/kg
Specific enthalpy of the off-coil air	32.2385	kJ/kg
Load on the coil	34.4695	kW
Apparatus dew-point moisture content	0.0077	
Apparatus dew-point temperature	10.4	C
Apparatus dew-point enthalpy	29.9	kJ/kg
Coil contact factor Eq1	0.88	
Coil contact factor Eq2	0.88	
Diff = Eq1-Eq2 = 0	0.0003	Goal
Use the solver to reach the goal		

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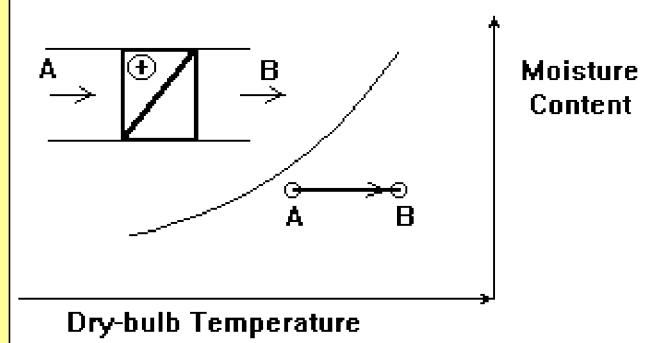
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## Appendix V

In an air conditioning plant, air flow rate of 2 kg/s passes through a heater battery. The dry-bulb temperature rises from 10 C to 24 C. The moisture content of the air is 0.005. Determine the load on the heater battery.



Inputs		Units
Inlet air, DBT	10.00	C
Inlet air, moisture content	0.005	
Inlet air, mass flow rate	2.00	kg/s
Outlet air, DBT	24.00	C
Outlet air, moisture content	0.005	
Outlet air, mass flow rate	2.00	kg/s
Outputs		
Specific enthalpy of the inlet air	22.6280	kJ/kg
Specific enthalpy of the outlet air	36.7503	kJ/kg
Load on the heater battery	28.2446	kW

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## Appendix W

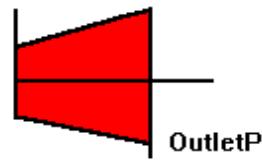
Superheated steam is supplied at 40 bar and 350 C to a single-stage turbine and the condenser pressure is 0.035 bar.

1-Calculate the output power of the turbine if the mass flow of steam is

2 kg/s and the isentropic efficiency of the turbine is 0.9

2-Calculate the dryness fraction at outlet

InletP & InletT



Inputs		Units	Error ?
Inlet Pressure/Admission Data	40	bar	
Inlet Temperature/Admission Data	350	C	
Outlet Pressure	0.035	bar	
Isentropic Efficiency	0.9		
Mass Flow	2	kg/s	
Outputs			
Inlet Enthalpy	3095.08	kJ/kg	
Inlet Entropy	6.59	kJ/(kg.K)	
Enthropy of Isentropic Expansion	1969.79	kJ/(kg.K)	
Outlet Enthalpy	2082.32	kJ/kg	
Output Power	2025.53	kW	
Dryness Fraction at Outlet	0.81		

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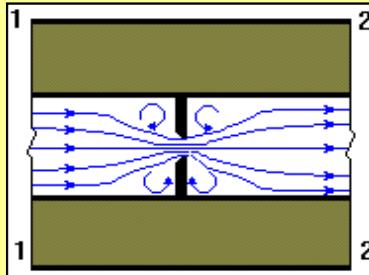
## Throttling Process

### Appendix X

Steam at 7.5 bar with 0.95 dryness fraction is throttled to 4.0 bar. Calculate the specific enthalpy, specific entropy, specific volume and temperature

1- at inlet  
2- at outlet

What is the dryness fraction at outlet?



Inputs		Units	Error ?
Inlet Pressure	7.50	bar	
Inlet Dryness Fraction	0.95	C	
Outlet Pressure	4.00	bar	
Outputs			
Inlet Enthalpy	2662.06	kJ/kg	
Inlet Entropy	6.4486	kJ/(kg.K)	
Inlet Specific Volume	242.7108	m <sup>3</sup> /ton	
Inlet Temperature	167.76	C	
Outlet Enthalpy	2662.06	kJ/kg	
Output Entropy	6.7130	kJ/(kg.K)	
Output Specific Volume	445.8866	m <sup>3</sup> /ton	
Output Temperature	143.62	C	
Dryness Fraction at Outlet	0.9646		

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